

Natural and Metamaterial Low-profile Antennas with Emphasis on Realization of Wideband Characteristics

- Antenna Height from $\lambda/4$ to $\lambda/100$ -

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Recent developments in communication systems, e.g.,
Mobile, Digital TV, and Satellite Communication Systems,
require

Antennas

with

**Dual-, Multi-, Moderately Wide-, and Extremely Wide-
Band Operation**

-:: categorized as either

Natural Antenna or Metamaterial (MTM) Antenna

**Natural Antenna / EM Property Found in Nature
(Right-Handed Property)**

**MTM Antenna / EM Property not Existing in Nature
(Left-Handed Property)**

Choice of either a **Natural** or an **MTM** Antenna depends on the requirements of the target communications system.

TALK PRESENTATION

recent progress in some

Natural and MTM Antennas.

Low-Profile Structure

realizing

Moderately wideband characteristics

Wideband characteristics

Extremely wideband characteristics

Key Words ::

Low Profile Structure

Wideband Characteristics

Out line

Section I Introduction

Section II Natural TW antennas

II-A Low-profile, moderately wideband **helical antenna**

II-B Extremely wideband **fan-shaped antennas**
for a base-station and a portable handset

II-C Low-profile, extremely wideband ***BOR-SPR antenna**
for a base-station antenna

***Body of Revolution with a Shorted Parasitic Ring**

II-D Low-profile, wideband **rhombic grid array antenna**
for frequency beam-scanning

Section III Metamaterial TW antennas

III-A History of the antenna height reduction of a spiral antenna

III-B Extremely low-profile, moderately wideband **spiral antenna**
for counter CP radiation

Section IV Remarks

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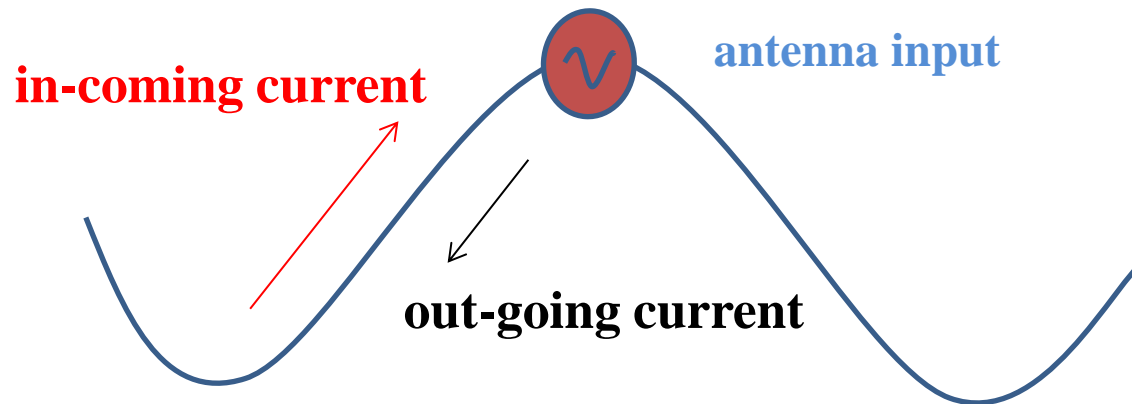
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(Current Distribution along Antenna Arms)*

Practical Antenna Arms // a Finite Length,

Current : composed of *

an out-going current & an in-coming current

The in-coming current

changes the situation at the antenna input.

~ changes **the antenna input impedance** in response to
the **antenna shape & operating frequency.**

.. Reduce the In-coming Current &

.. Use Only the

Out-Going Traveling Wave (TW) Current

to Realize Wide Band Antennas

-.: categorized as either

Positive- β TW current

or

Negative- β TW current.

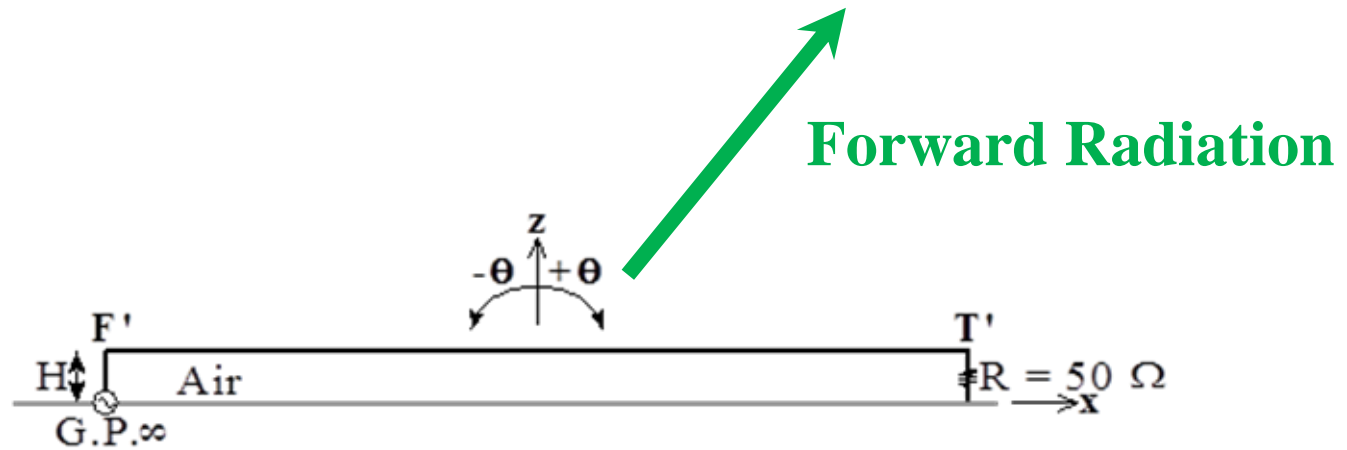
Antenna based on a positive- β TW current : defined as*

Natural (TW) Antenna*

Antenna based on a negative- β TW current : defined as

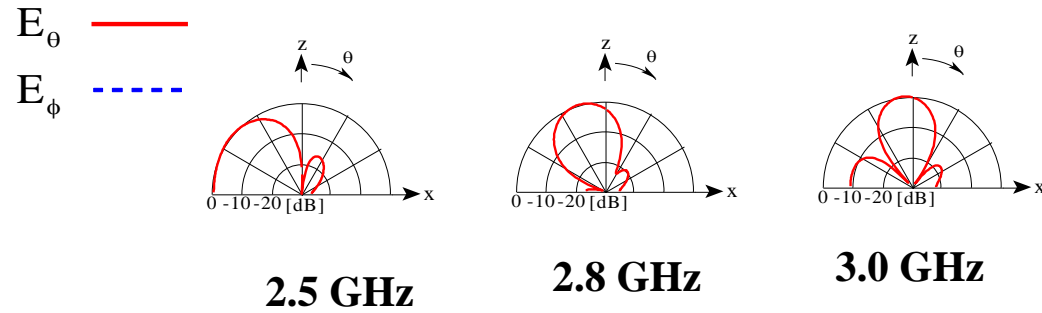
Metamaterial (TW) Antenna

Example of a Natural TW Antenna

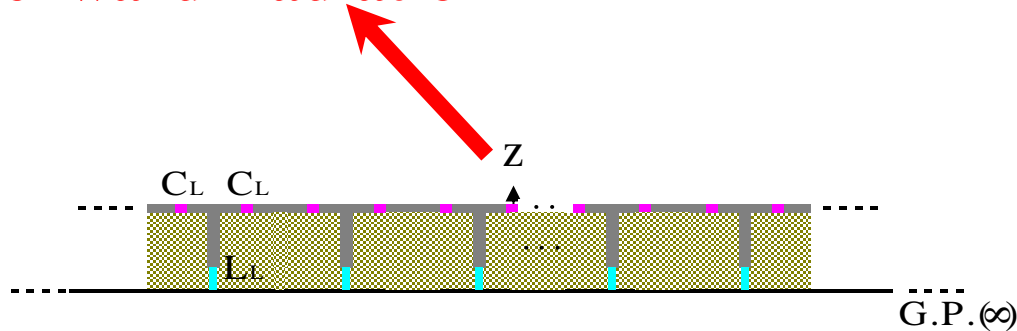


- - **A positive- β current flows from F' to T'**
A Phase-Lag Based on a positive- β Current
Forward Radiation*

***Example of a MTM TW Antenna**



Backward Radiation



- - Capacitances and Inductances ::
inserted into a microstrip line*

A negative- β current flows from the left to the right.

A Phase-Progress Based on a Negative- β Current

Backward Radiation

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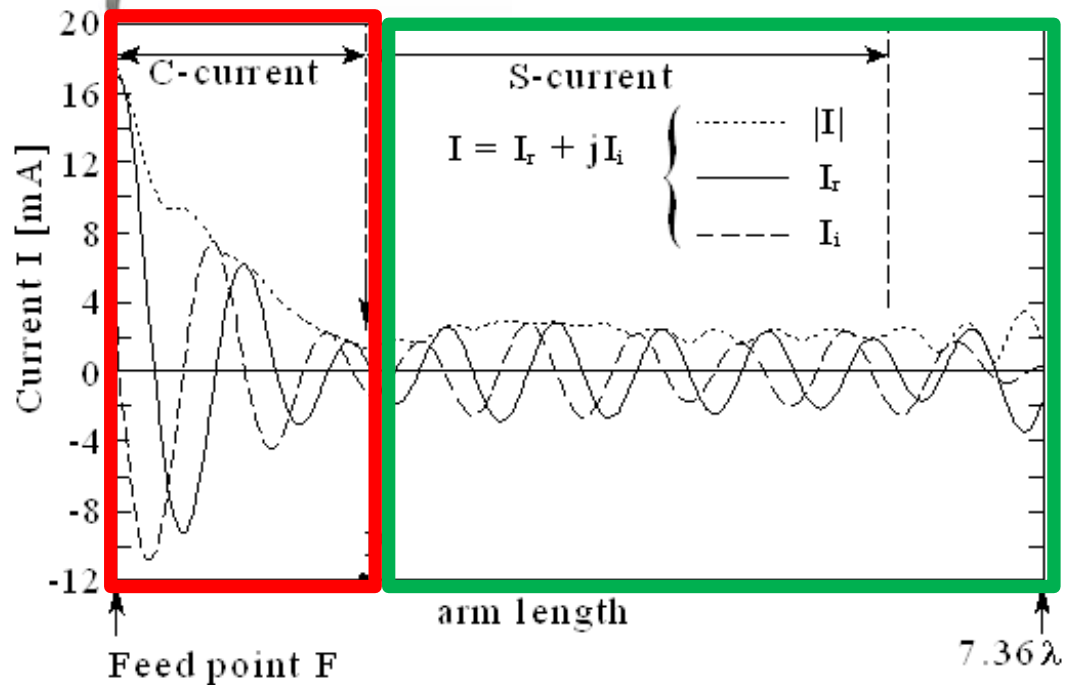
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Helical Antenna



FINDING

Current /

two distinct regions

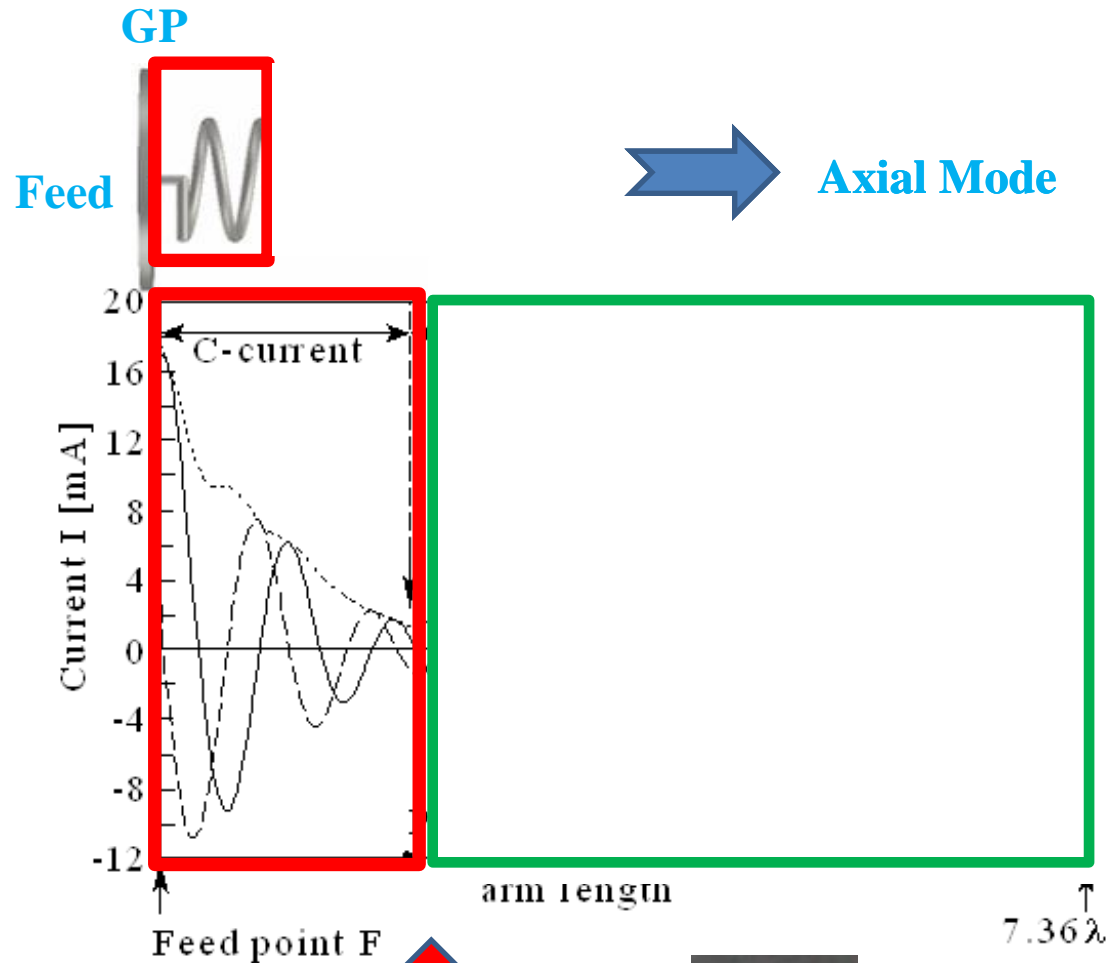
C-current region* &

S-current region*

.. Remove the S-current region* &
.. use only the C-current region
for CP radiation

-/ a decaying TW current
along the helical arm of
~ two turns* *

~ an antenna height of
0.19 wavelength
above the GP



2 turns



*Application of Low-Profile Helical Element

Each element : arrayed on a cavity

Vertical line of the helix : inserted into a cavity* &
excited by a traveling EM wave*

Aperture Efficiency :
extremely high and approx. 90%.

**Aperture
Efficiency
~ 90%**

Phase :
controlled by rotating the element
around its axis.

Amplitude :
controlled by the vertical length
inserted into the cavity.

Circular cavity

Side view of a cavity

13

ARRAY /: used as

Indoor Broadcasting Satellite Receiving Antenna



Dia. = 27.8 cm
G = 29.5 dBi,



Designed by Nakano Lab
Produced by Yagi Antenna Co.



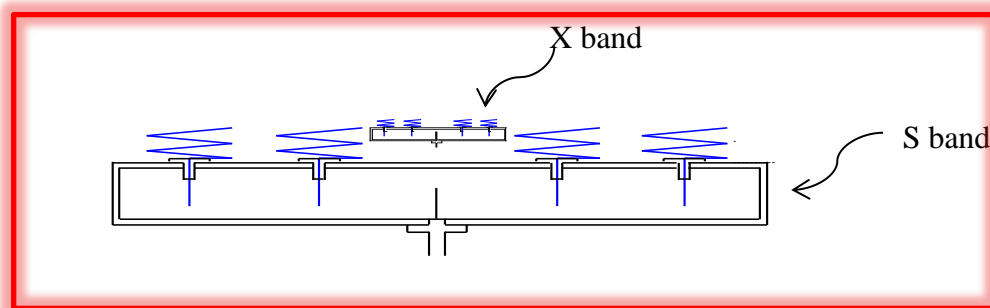
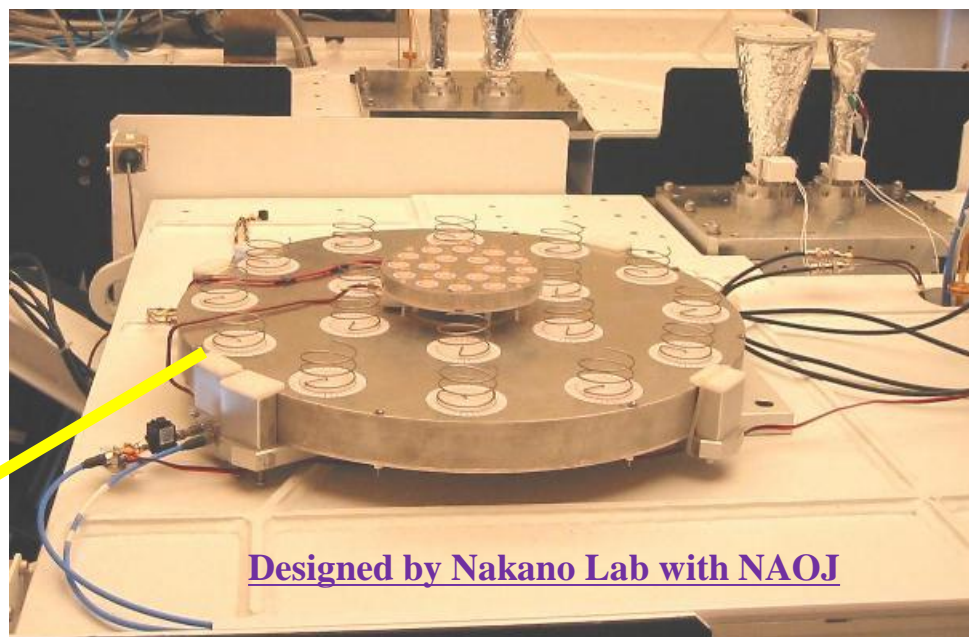
/ Dia. = 33 cm
G = 31.7 dBi,
Aperture efficiency of $\eta = 88\%$

Designed by Nakano Lab
Produced by TDK Co.

Cassegrain reflector /

a main dish of diameter of 20 m * &
a sub-dish of diameter of 2.6 m.

Focal length of main dish : 6 m. *



Primary feed / a two-layer structure.

X band (8.1-8.9 GHz, BW = 9.4%).

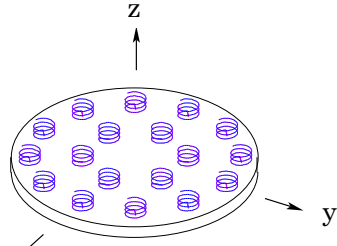
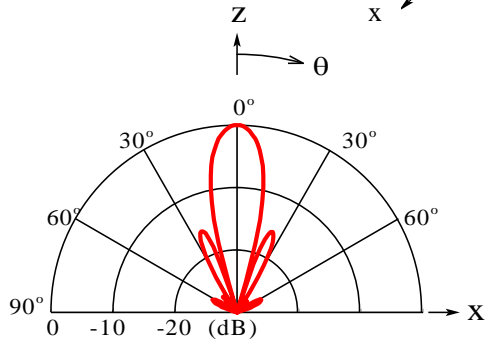
S band (2.1-2.6 GHz, BW = 21.3%)

Helical elements: plated with Gold

<http://veraserver.mtk.nao.ac.jp/restricted/status05.pdf> (Japanese)

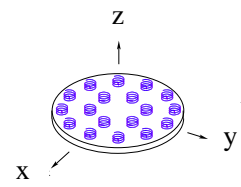
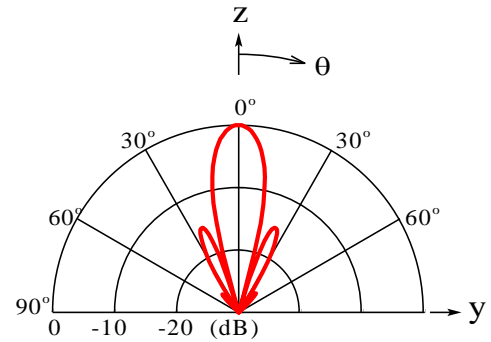
Radiation Pattern

— E_R
 - - - E_L



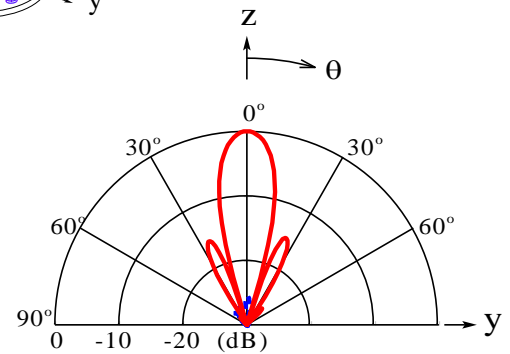
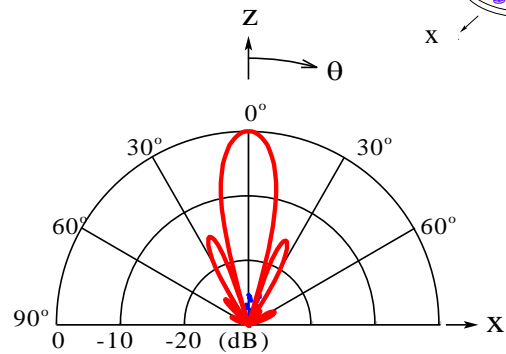
S Band

$f = 2.35 \text{ GHz}$



X Band

$f = 8.55 \text{ GHz}$



The same beam width is realized.

A beam width of 22° for a 7-dB reduced field intensity criterion is realized, meeting the requirement for both of the feed antennas.

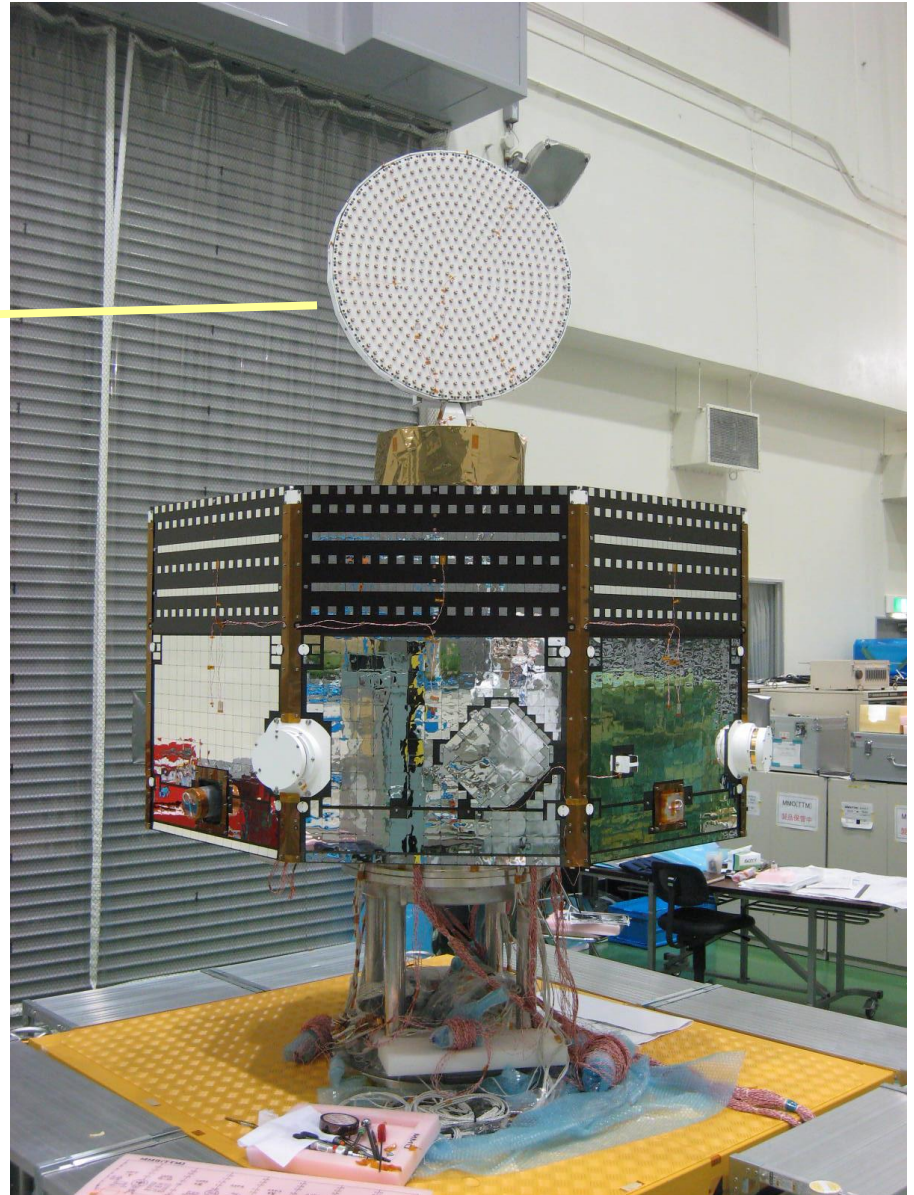
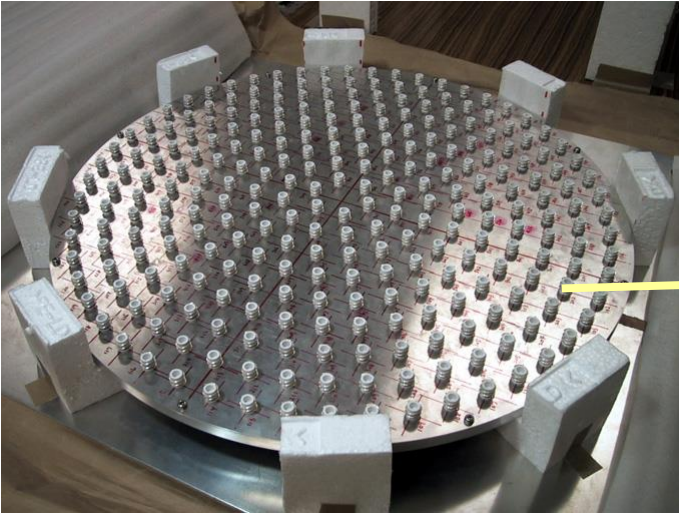
Symbol	Value
D_{HLX}	41.38 mm $\approx 0.3241\lambda_{2.35}$
n	3.1 turns
α	4°
ρ	0.5 mm $\approx 3.917 \times 10^{-3} \lambda_{2.35}$
H_{CAV}	495 mm $\approx 3.8775\lambda_{2.35}$
D_{CAV}	36 mm $\approx 0.282\lambda_{2.35}$
S_{cir}	109 mm $\approx 0.8538\lambda_{2.35}$
S_{rad}	104 mm $\approx 0.8147\lambda_{2.35}$

* $\lambda_{2.35} \approx 127.66 \text{ mm}$

Symbol	Value
D_{HLX}	11.169 mm $\approx 0.3183\lambda_{8.55}$
n	2.8 turns
α	4°
ρ	0.2 mm $\approx 5.7 \times 10^{-3} \lambda_{8.55}$
H_{CAV}	142 mm $\approx 4.047\lambda_{8.55}$
D_{CAV}	9.7 mm $\approx 0.27645\lambda_{8.55}$
S_{cir}	29.4 mm $\approx 0.8379\lambda_{8.55}$
S_{rad}	28.1 mm $\approx 0.8009\lambda_{8.55}$

* $\lambda_{8.55} \approx 35.294 \text{ mm}$

*Helical antenna array for a **BepiColombo**



Presented by
JAXA and
NEC-TOSHIBA Space System

Out line

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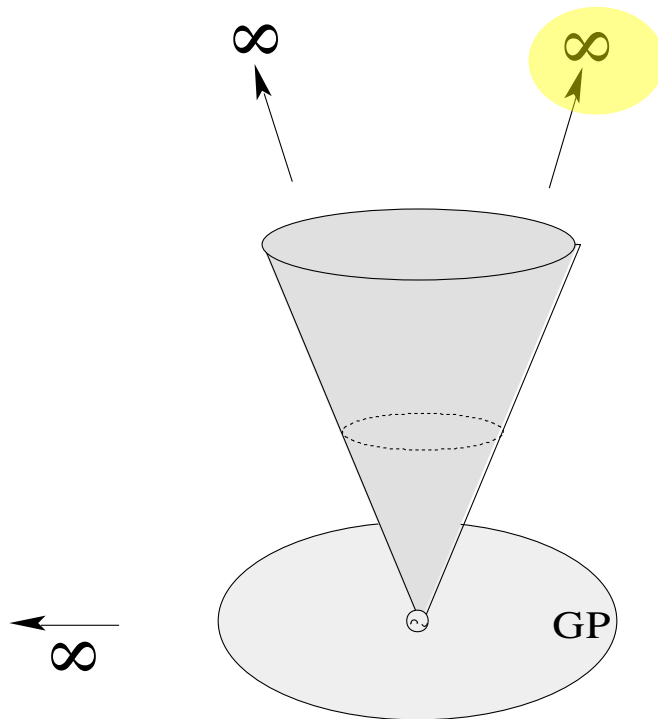
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*Conducting Conical Antenna



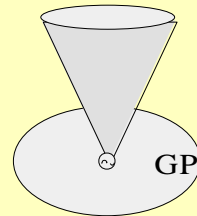
- / Only an Out-going Current
IF: Conical Arm: Infinitely Long &
Ground Plane : of Infinite Extent

**Input impedance :
Frequency-Independent***

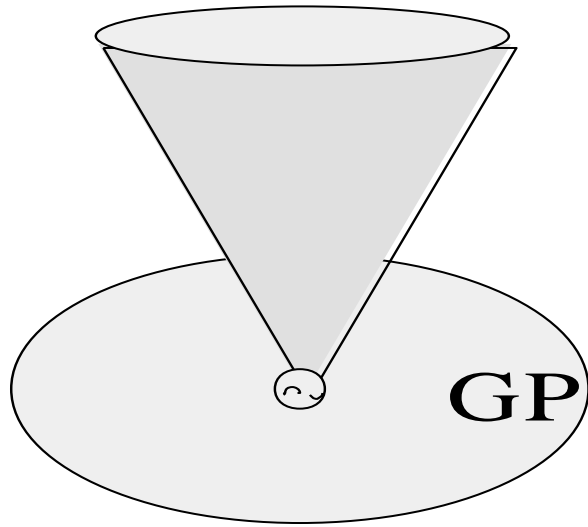
Practical Structure

//The Conical Arm Cannot Be Infinitely Long!

Practical Truncated Conical Antenna

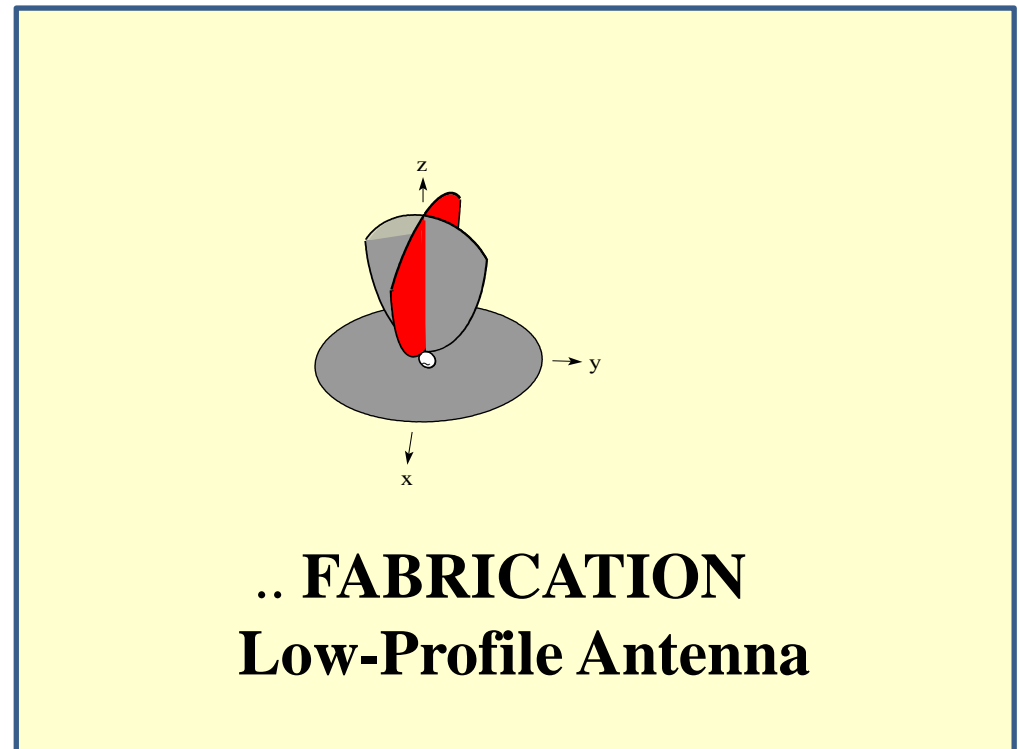


No More: Inherent Frequency-Independent Characteristics
// .. Expect Wideband Characteristics
- Partially Retains the Original Structure



**Truncated
Conical Antenna***

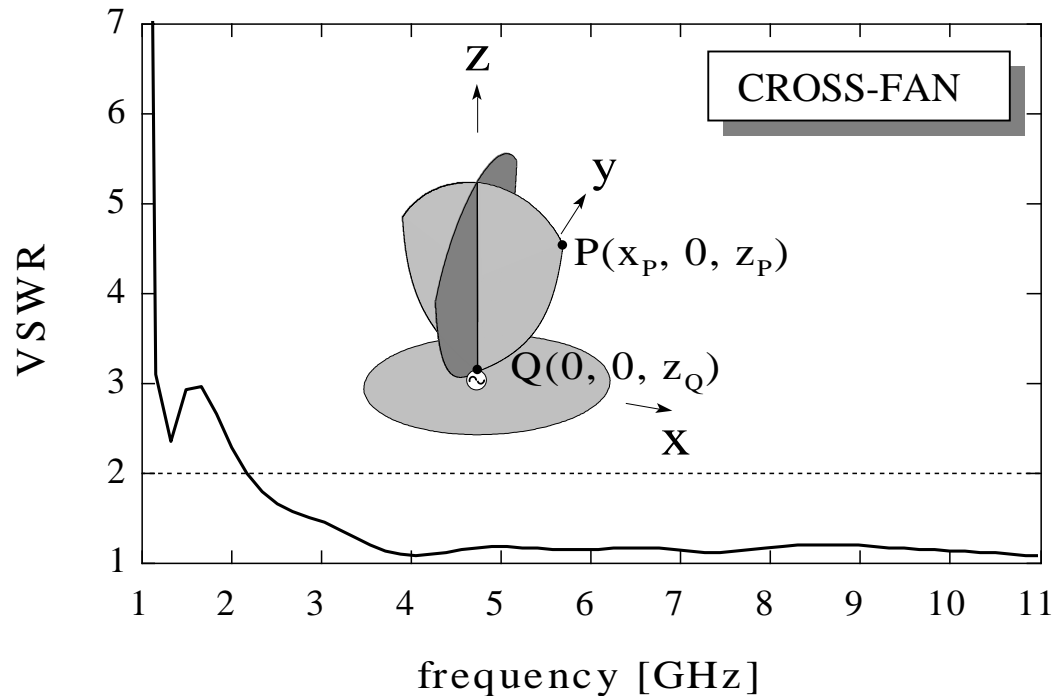
**Modification from a Truncated Conical to
A CROSS-FAN Antenna**



**.. FABRICATION
Low-Profile Antenna**

- - A Pair of Fan-Shaped Plates
Intersect at Right Angles*

*Frequency Response of the VSWR of the Cross-Fan Antenna



Antenna Height : 0.3 Wavelength at 2.1 GHz

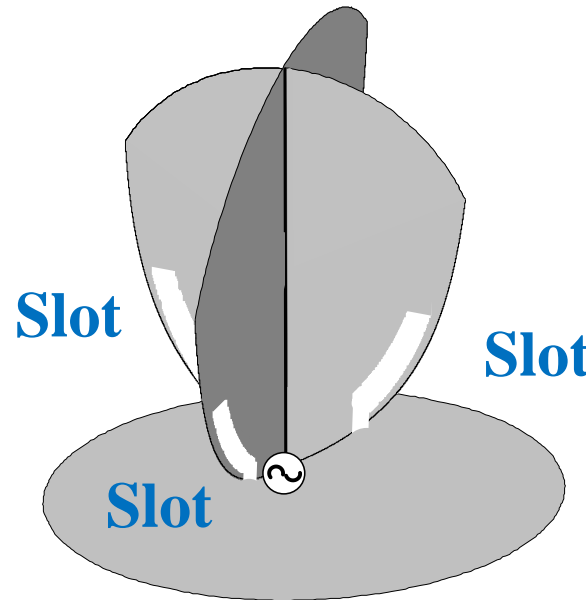
Note: VSWR : less than two at frequencies above 2.1 GHz*.

Antenna Height : 0.3 Wavelength at 2.1 GHz.

Radiation : Omnidirectional around the antenna axis (z-axis).

Technique for Stop-Band Generation

in order to prevent the reception of interference from nearby devices



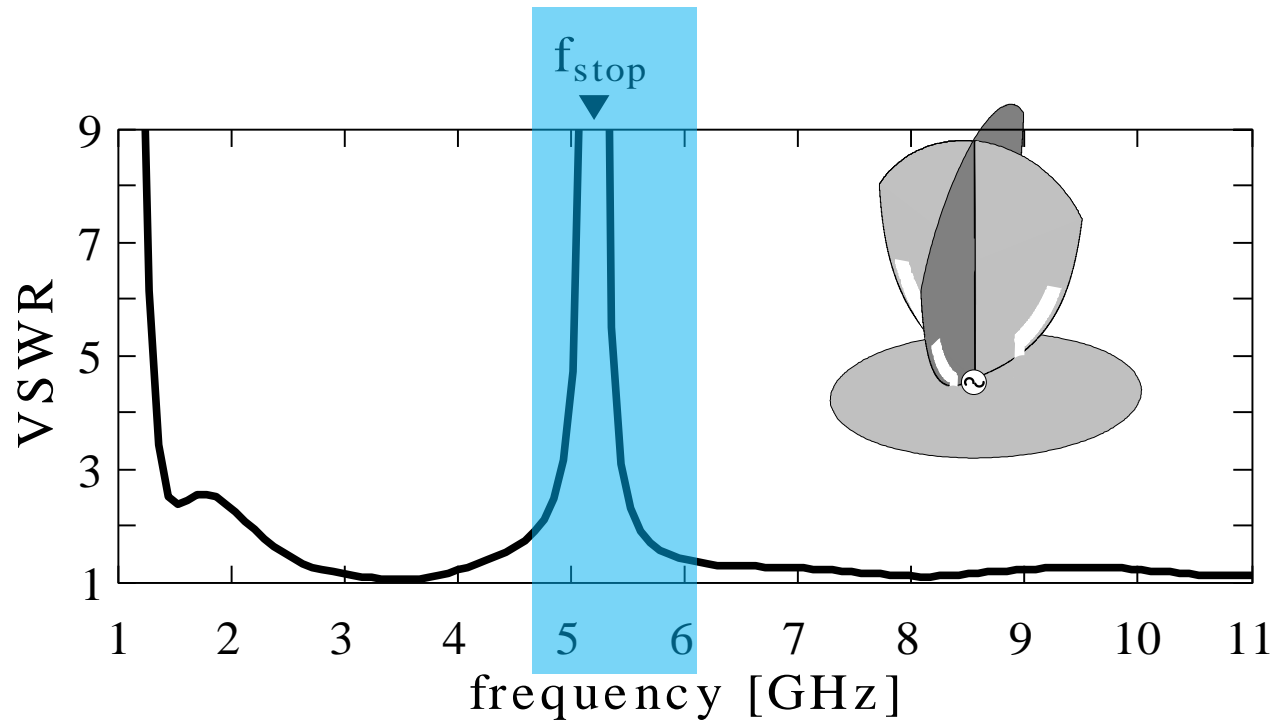
CROSS-FAN-SLOT
Requirement of Stop Band

Cross-fan : often required to have a stop band within the VSWR band \wedge

Introducing slots* into the fan-shaped plates : recommended.

This antenna : designated as the **CROSS-FAN-SLOT**.

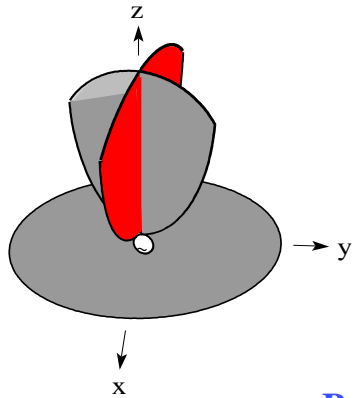
*VSWR of the CROSS-FAN-SLOT



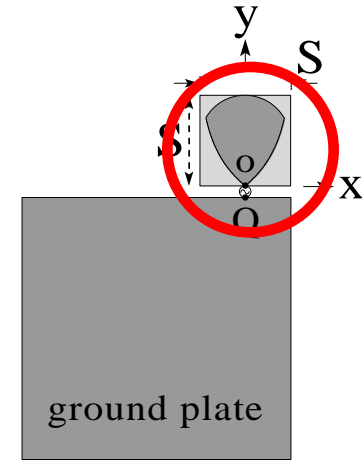
A Stop Band : * around 5.2 GHz

Slot Length L_{slot} : ~ one-quarter wavelength at f_{stop} .

As Slot Length L_{slot} ↑
Stop-Band Center Freq. f_{stop} *



Base Station Antenna >>> Portable Handset Antenna



Fan-shaped plate antenna

CROSS-FAN /: Used as a Base Station Antenna

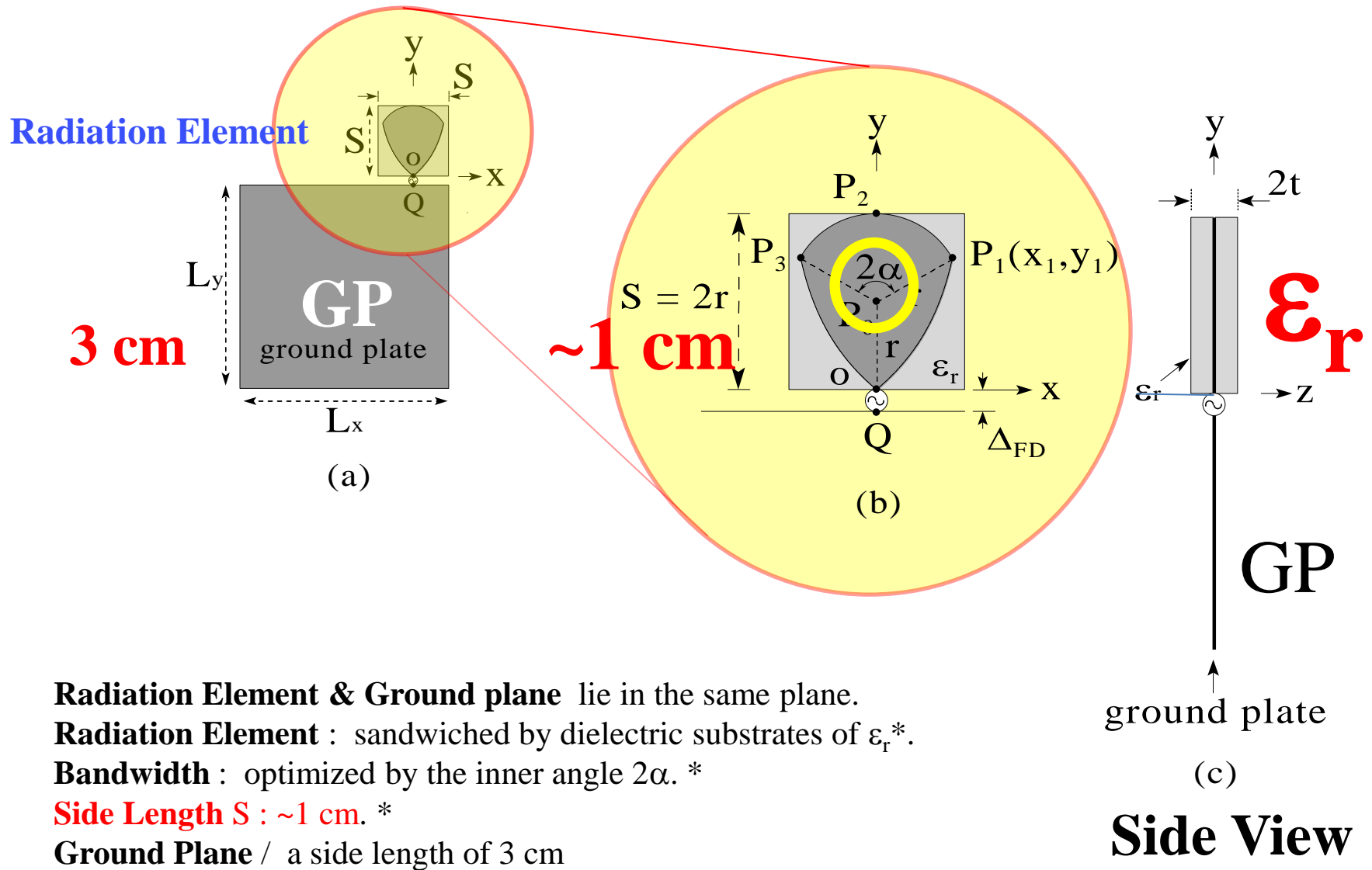
.. MODIFICATION CROSS-FAN for a **Portable Handset**

- REQUIREMENT **Card-type Structure**

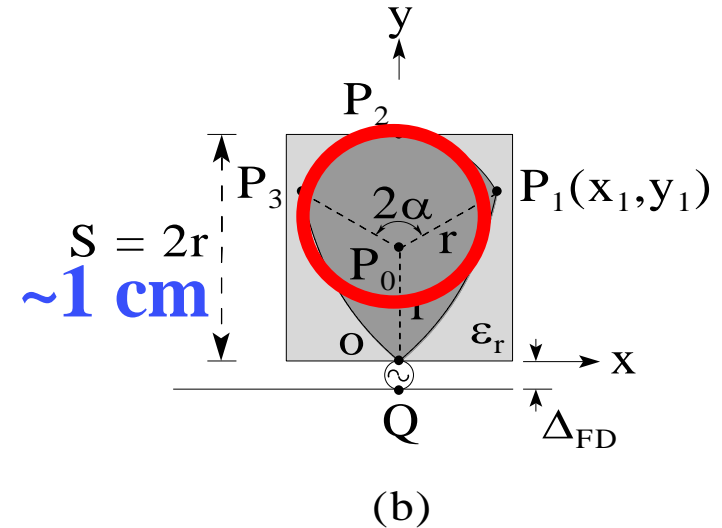
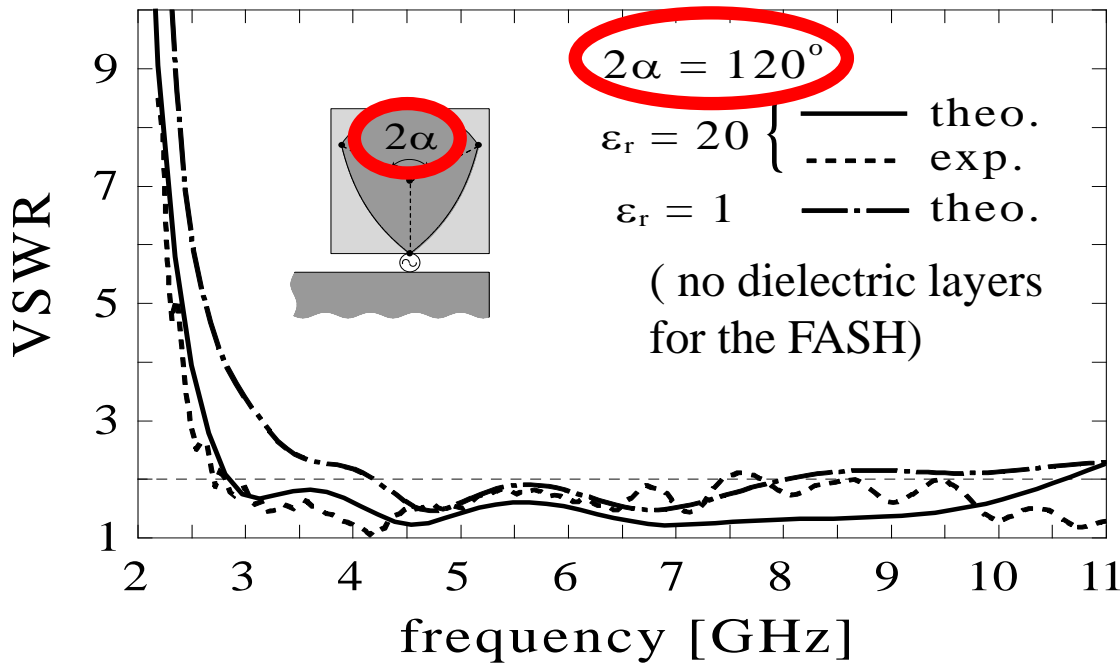
.. REDUCTION **Two fan-shaped plates to one plate ** &**

.. MAKE **Antenna Height Small - : Fan-shaped plate antenna**

*** Detail of fan-shaped plate Antenna**



*Frequency response of the VSWR

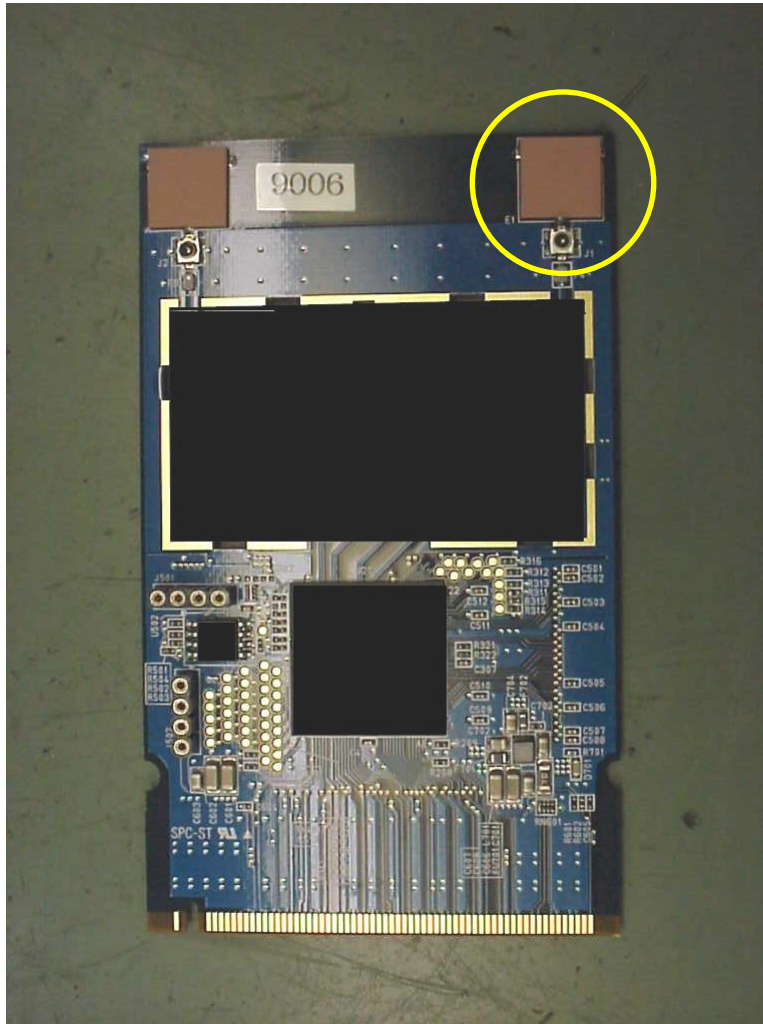


$2\alpha = 120$ degrees.
 $(\epsilon_r, 2t, S) = (20, 1 \text{ mm}, 10.87 \text{ mm}),$
 $(L_x, L_y) = (30 \text{ mm}, 30 \text{ mm}),$
 $r = 5.44 \text{ mm}$

Note: **VSWR < 2** above **2.75 GHz**.
Antenna Height : 0.09λ at 2.75 GHz.
Ground Plane / a side length of 3 cm

Installation of a Fan-Shaped Antenna *

II Natural Wideband Antennas.
II B CROSS-FAN and CROSS-FAN-S



- : Installed in a handset device. *
- : Sandwiched by dielectric substrates

Substrate /
an area of $\sim 1 \text{ cm} \times 1 \text{ cm}$.

Designed by Nakano Lab.
Produced by Mitsumi Co.

The substrate has an area of 1 cm by 1 cm.
The antennas installed inside a handset device.

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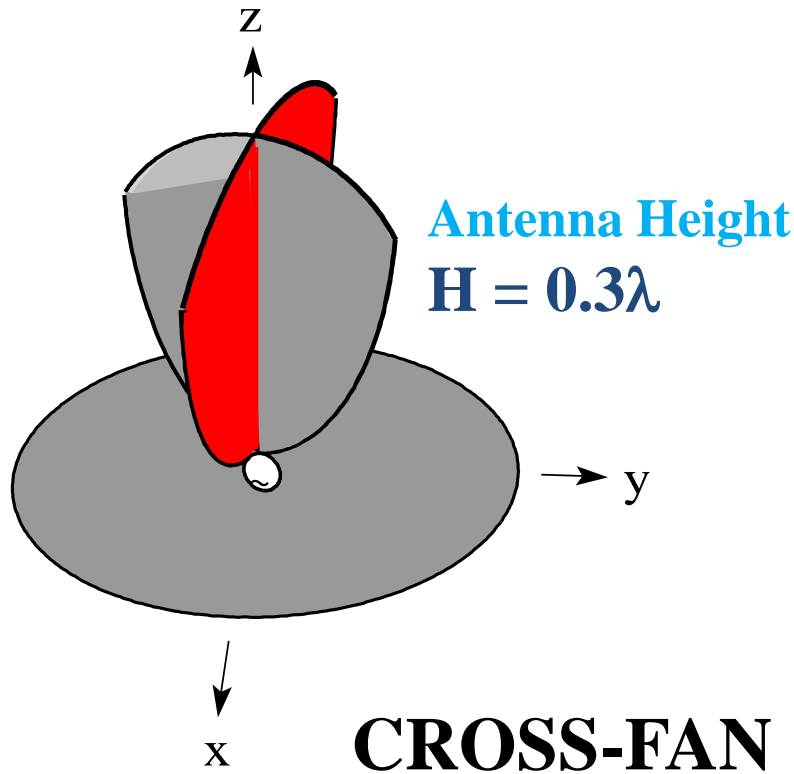
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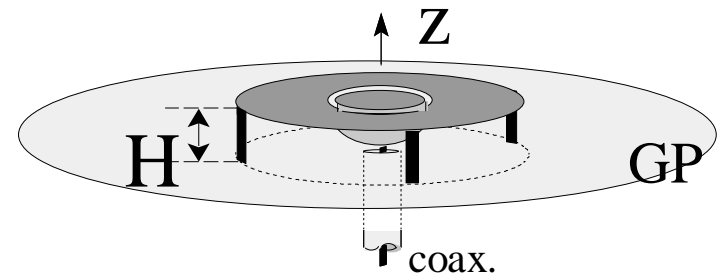
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→ Lower Base Station Antenna
 $H = 0.07\lambda$

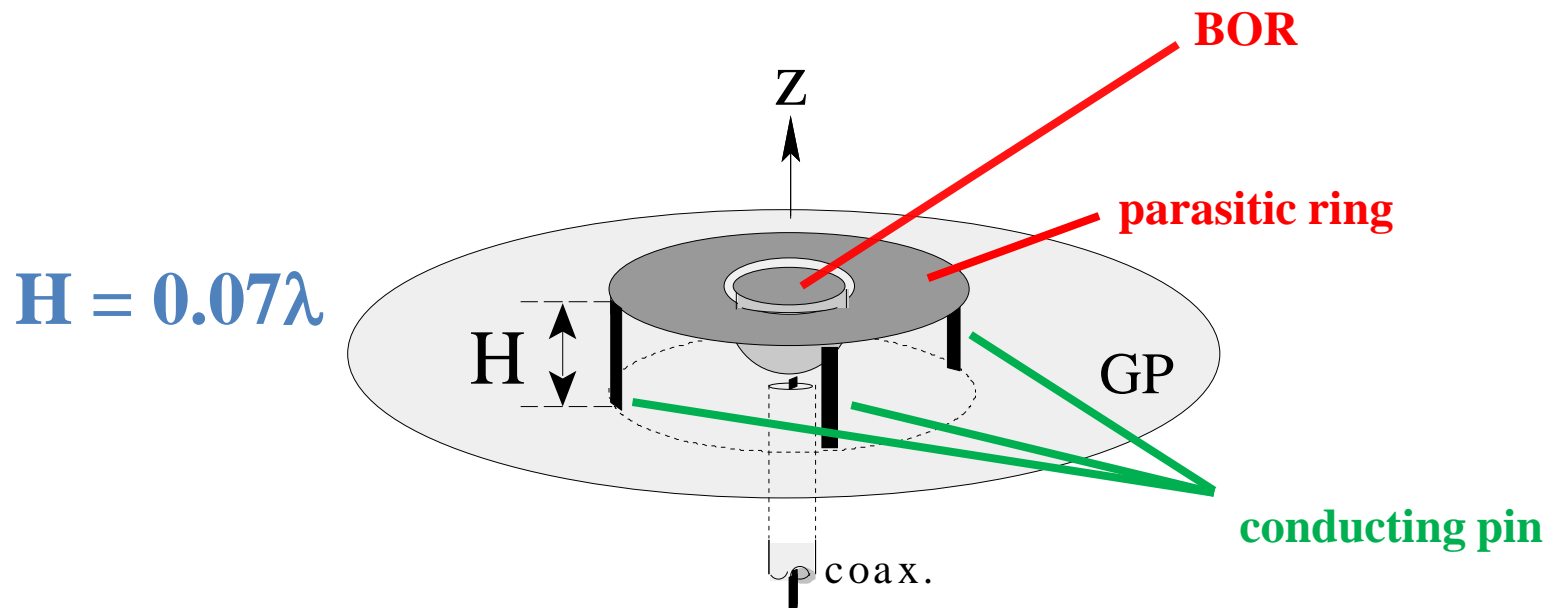


BOR-SPR

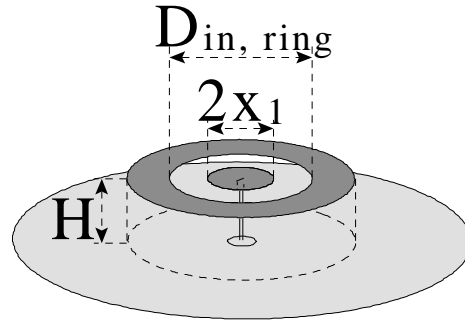
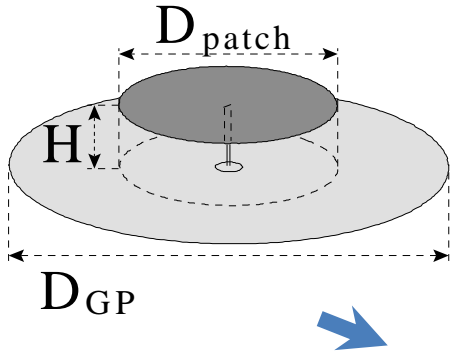
Body of Revolution with
a Shorted Parasitic Ring

BOR-SPR Base-station Antenna

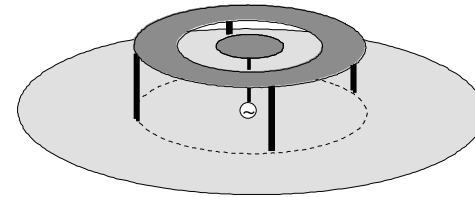
- ***BOR-SPR Antenna** : composed of
 - a conducting body of revolution (feed section) *
 - & a parasitic conducting ring* :
 - shorted to the ground plane through conducting pins *.
- Antenna Height** : extremely small*: 0.07 wavelength.



Design of BOR-SPA



.. Add four conducting pins.



.. Cut a ring slot



$$H = 0.07\lambda$$

Microstrip patch

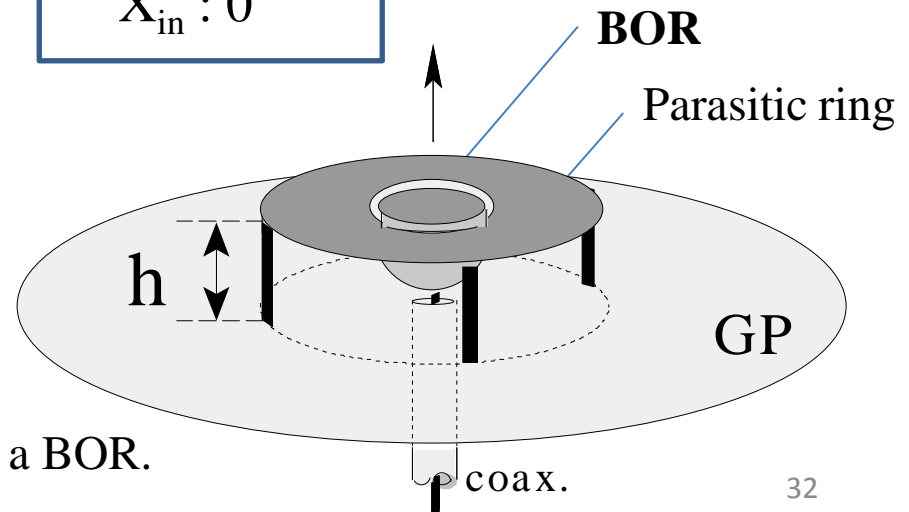
$R_{in} : \text{low} < 50$ $X_{in} : \text{inductive}$



$R_{in} : \text{low} < 50$ $X_{in} : 0$
--



$R_{in} : 50$ $X_{in} : 0$

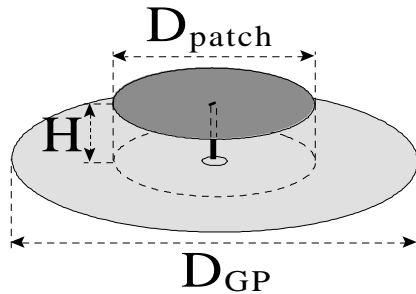


.. Replace the feed section by a BOR.

Design Process

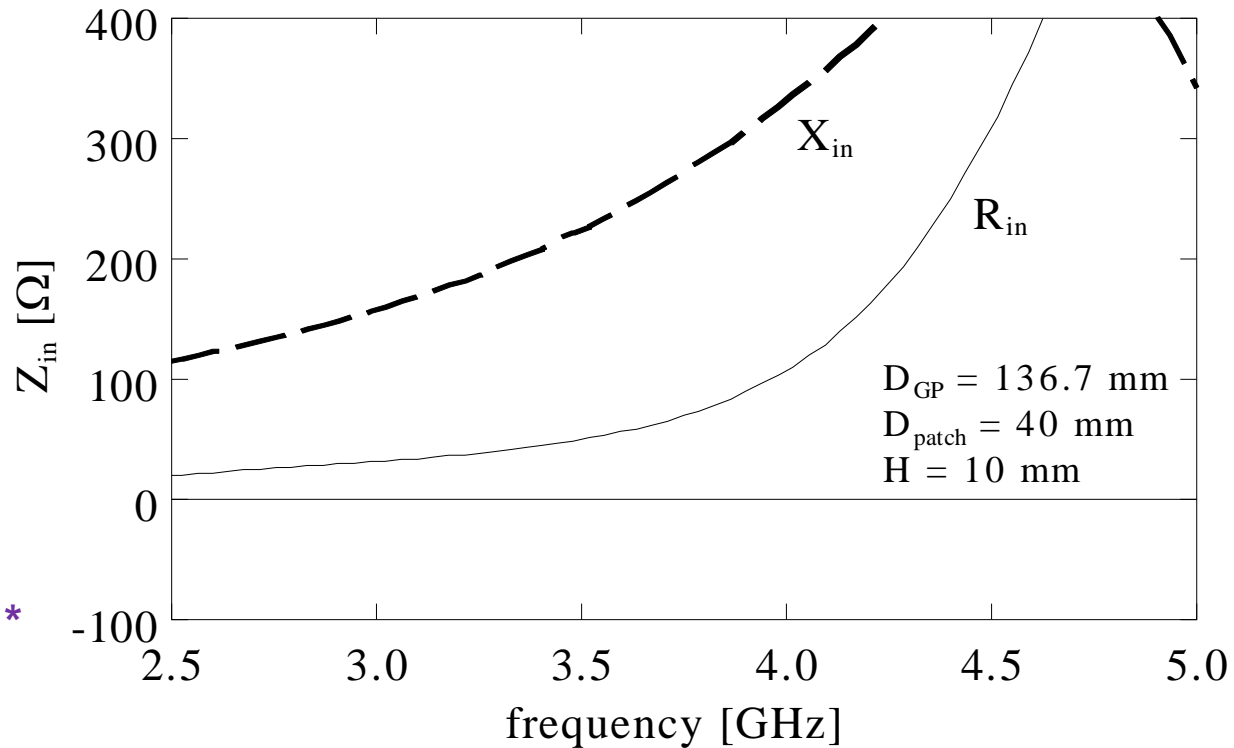
First Step : to analyze the input impedance for a low-profile patch

Patch dia. ~ 4 cm



GP dia. ~ 14 cm

Antenna height $H = 1 \text{ cm}^*$



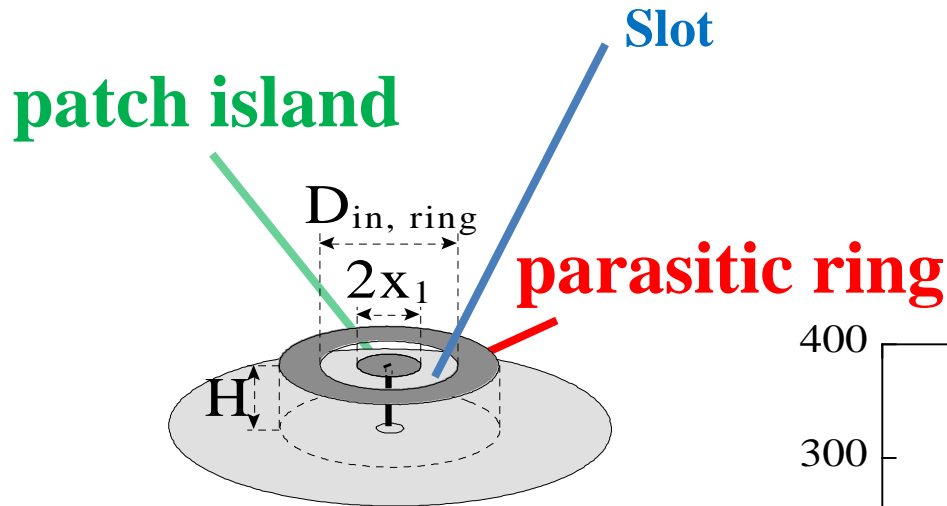
$R_{in} < 50 \text{ ohms}$

X_{in} : inductive

Note:

There is a frequency region where the input reactance X_{in} is highly inductive.

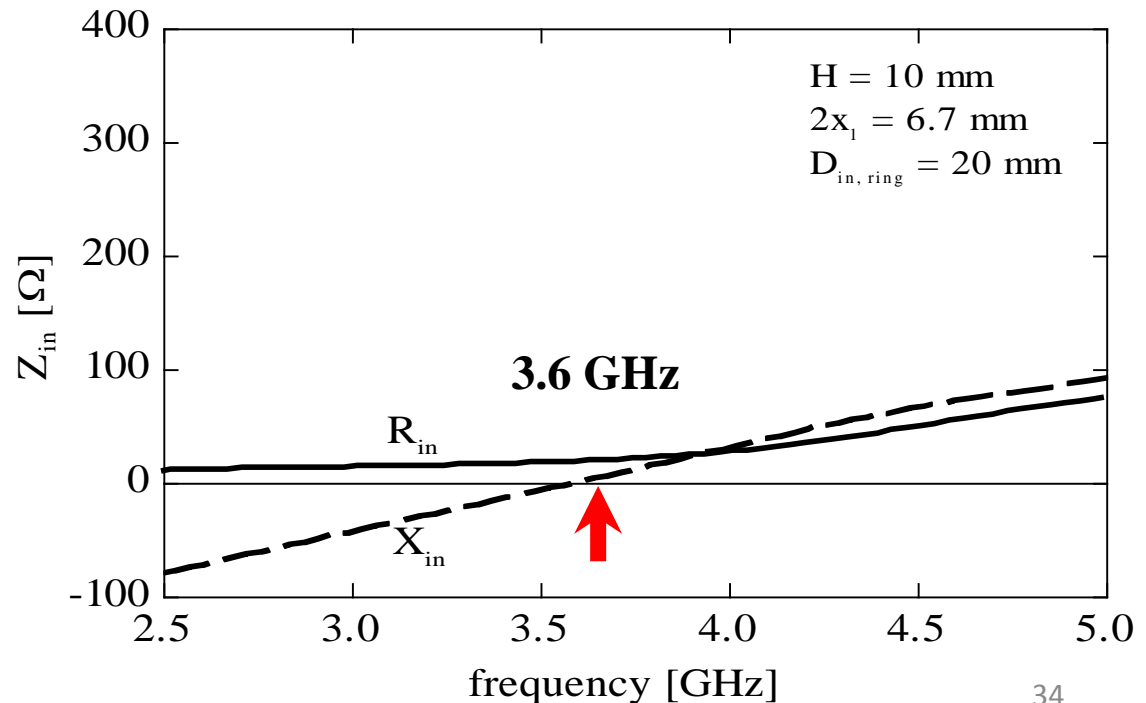
Second step : To make the input reactance X_{in} zero by adding a **capacitive component**.



R_{in} : low < 50
 X_{in} : **0**

: performed by cutting a ring slot into the original patch.*
 The slot forms a capacitance.

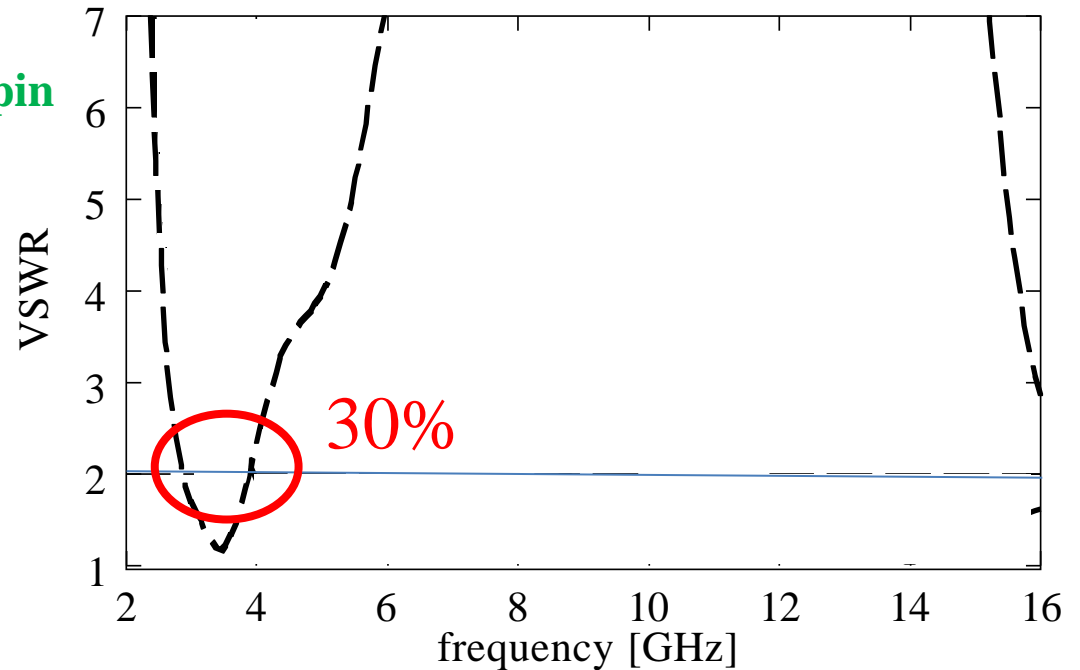
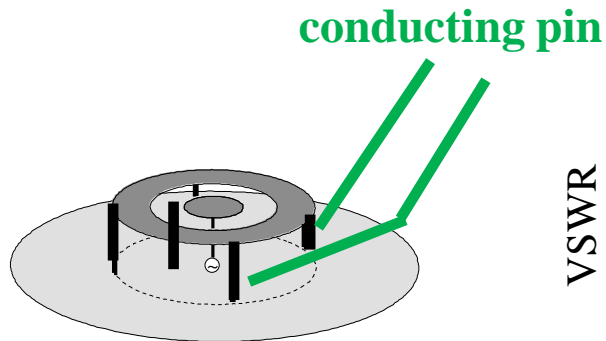
The original patch : divided into two regions, parasitic ring region* & small patch island*



Third Step :To increase the input resistance R_{in} .

: achieved by increasing the antenna volume.

: performed by adding conducting pins & short them to the ground plane*.



R_{in} : increased to **50 ohms**

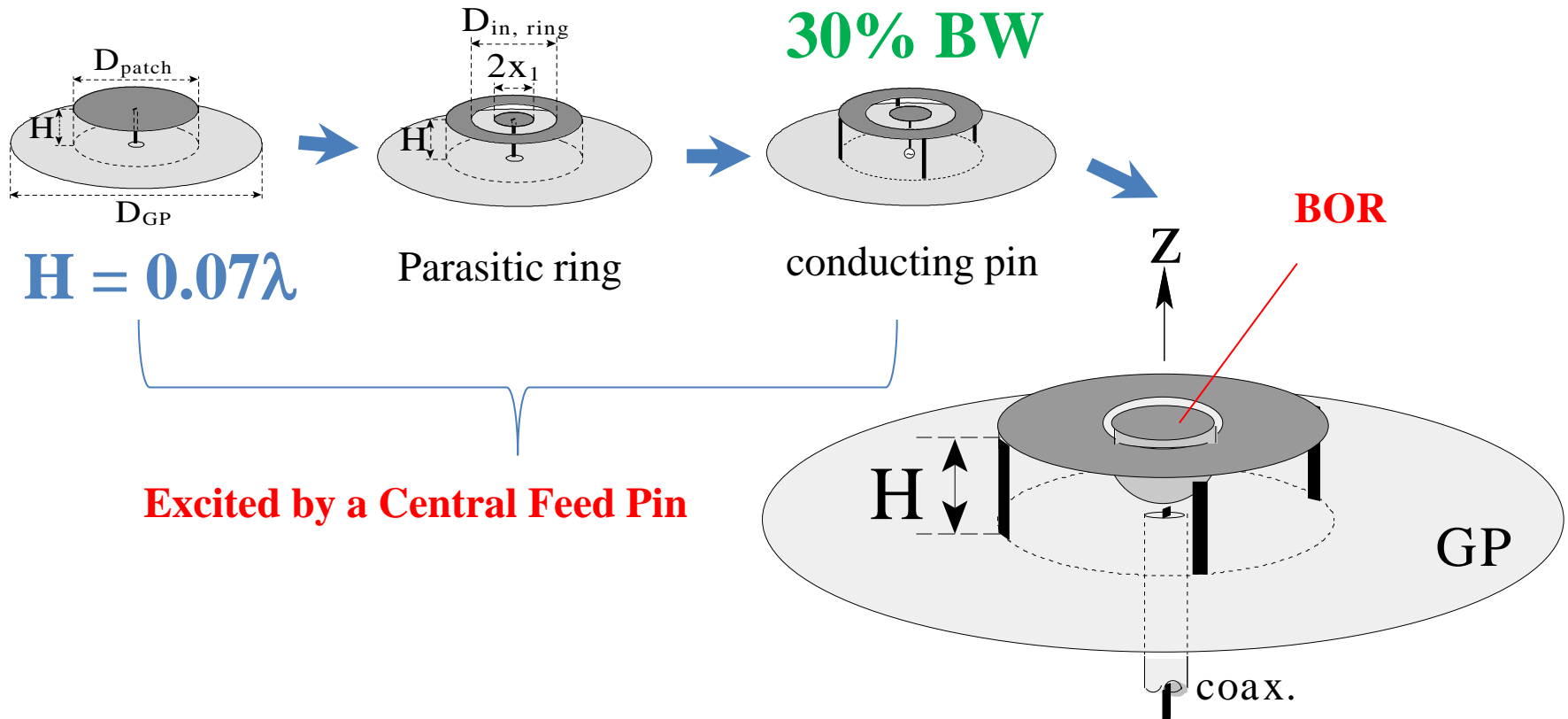
X_{in} : 0

Final Step : To further increase the frequency BW.

Antenna: excited by a central feed pin *

Central feed pin : replaced by a **conducting body of revolution.***

Generating line of the BOR : defined by an exponential function.



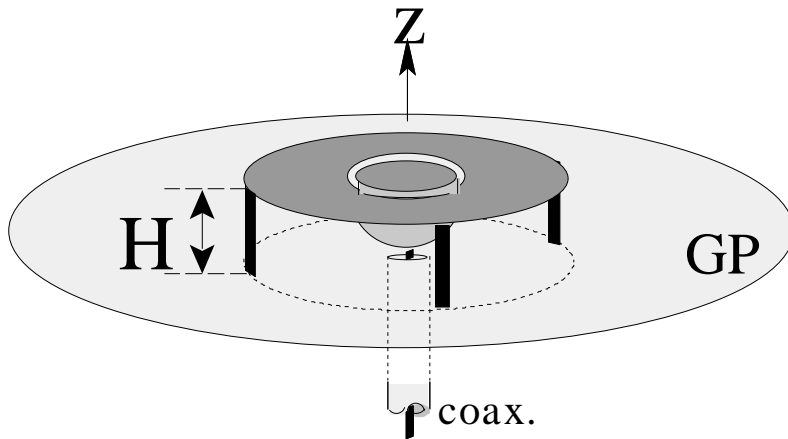
* Frequency response of the VSWR for the BOR-SPR.

An extremely-wide frequency-band of

147% *

Note: The radiation :

omnidirectional around the z-axis.

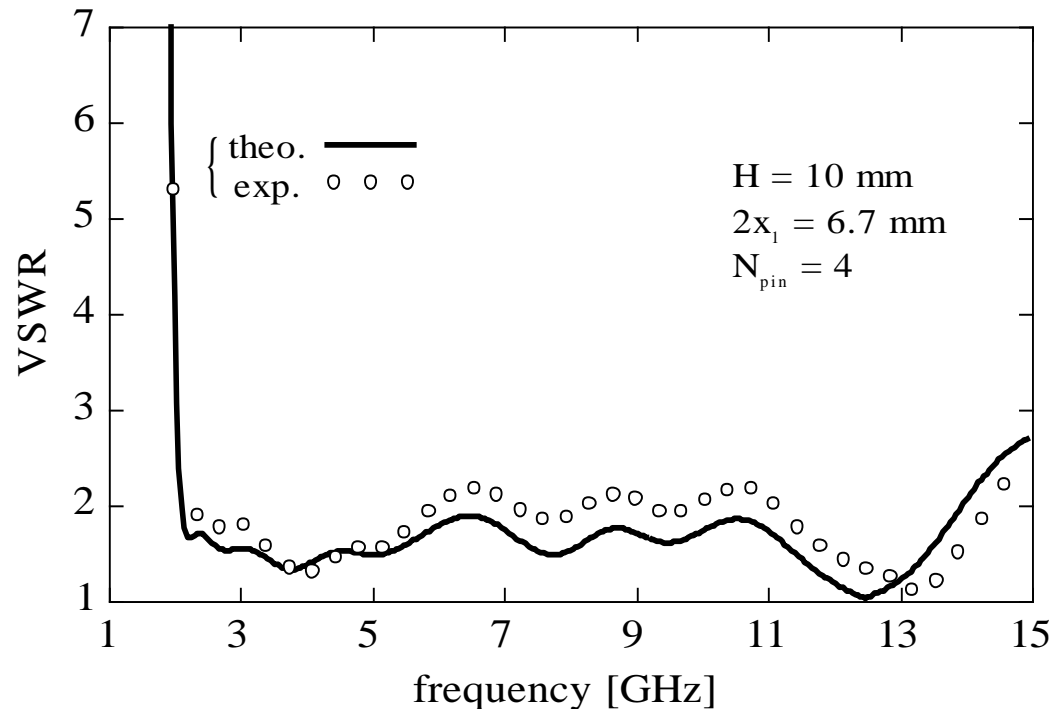


$$H = 0.07\lambda$$

$$r_{\text{patch}} = 0.13\lambda$$

BOR-SPR

Body of Revolution with
Shorted Parasitic Ring



147% BW

*Installation example
of BOR-CROSS*



**Designed by Nakano Lab.
Produced by Yagi Antenna Co.**

BOR-CROSS is installed on the ceiling of a building.

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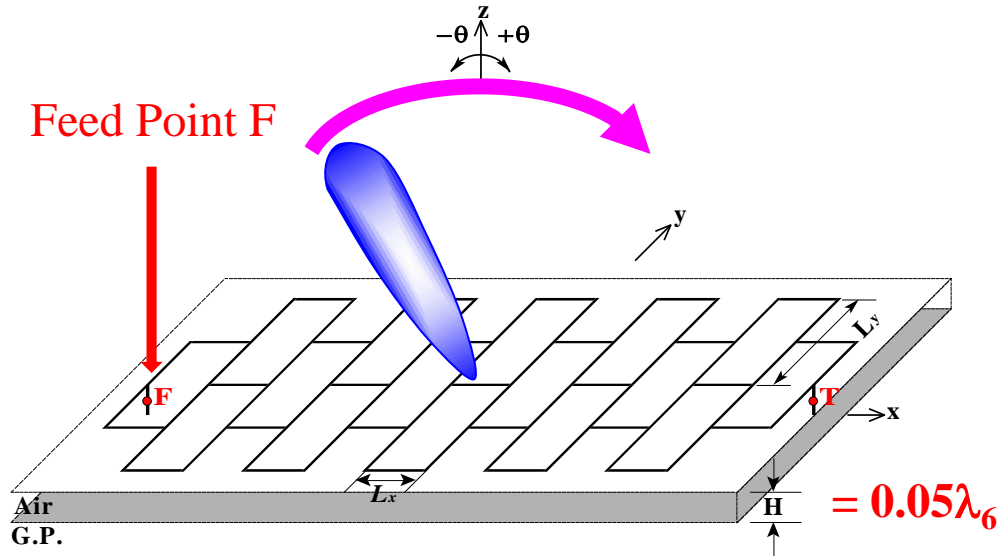
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for counter CP radiation

Section IV Remarks

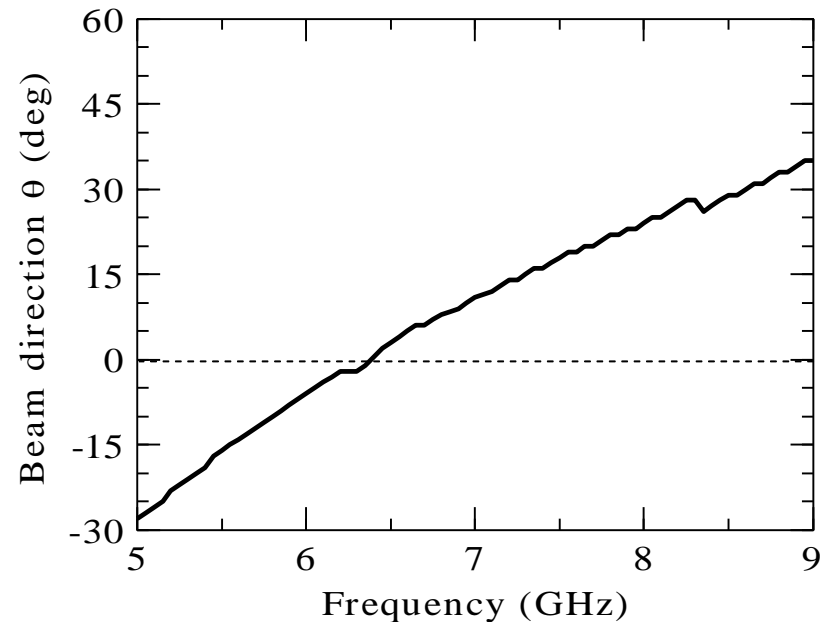
*Conventional Grid Array Antenna (GAA)



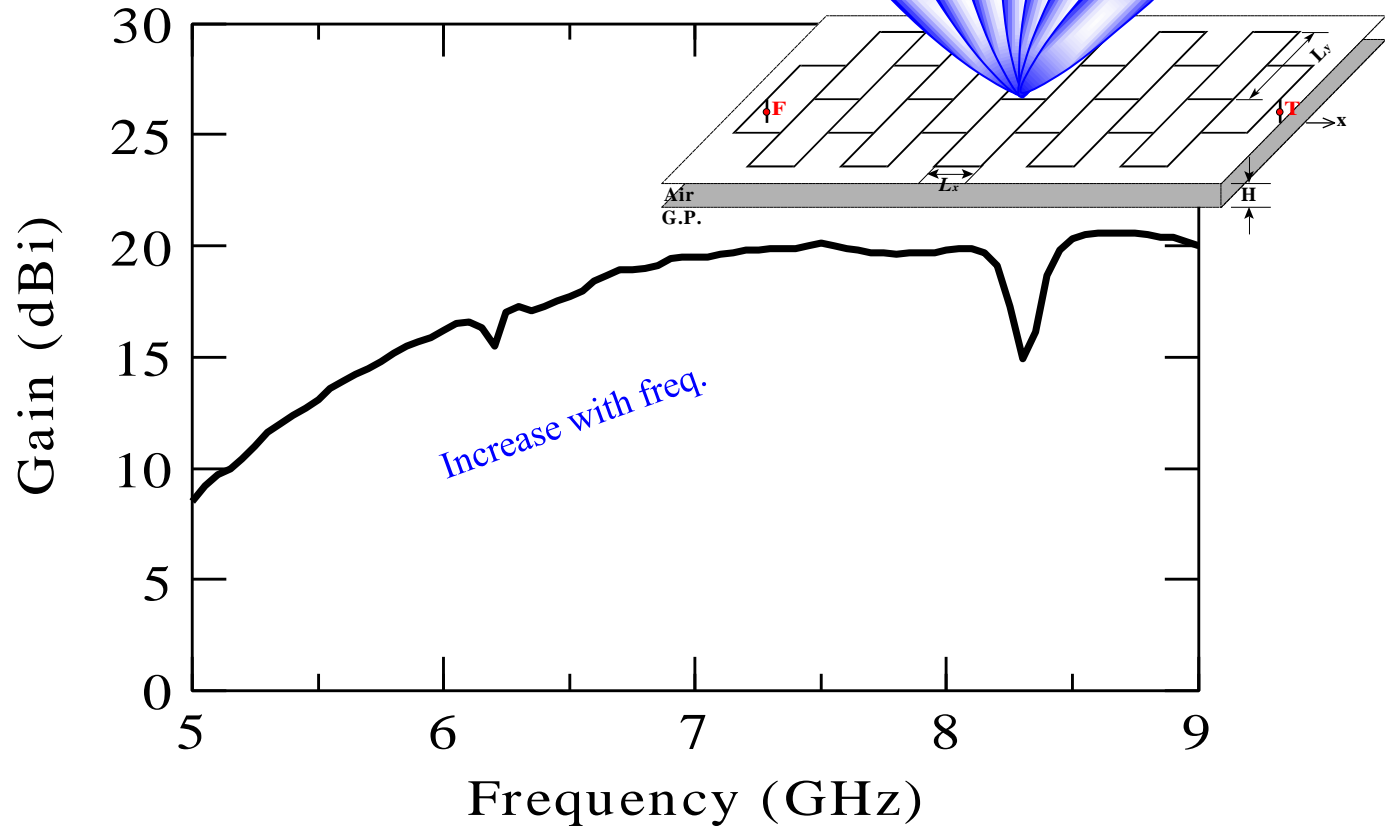
**Antenna height $H = 2.5 \text{ mm}$
 $= 0.05\lambda_6$**

GAA : excited from its edge*
 - creates a tilted beam* *Beam direction*
 / a frequency-scanning function.

*Beam Direction
 as a function of frequency.



?? Gain of the conventional GAA ??



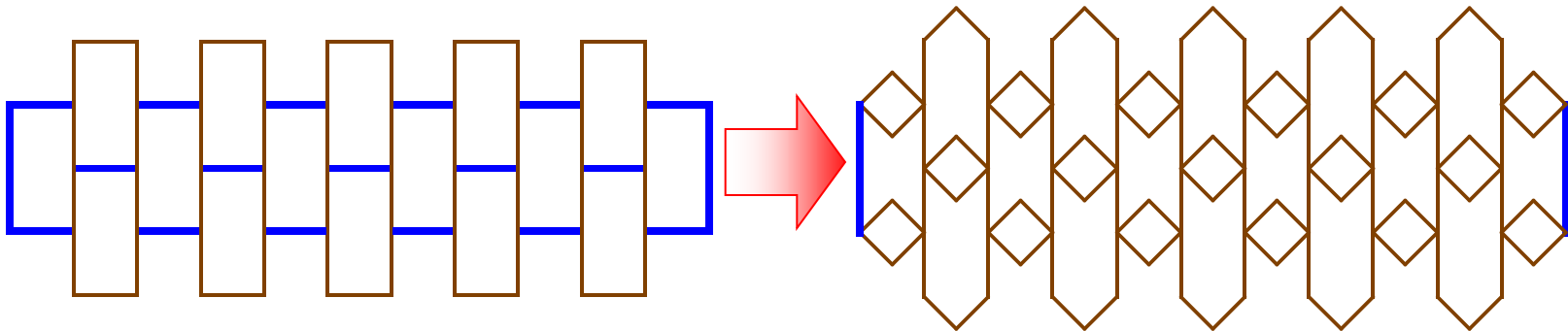
?Desirable Gain Behavior?

The gain should be constant

across the wide frequency band to be used for beam scanning.

As one solution to this issue*,

.. Propose a New Grid Array Antenna*



Conventional

Proposed

-: Rhombic GAA

Proposed RGAA :

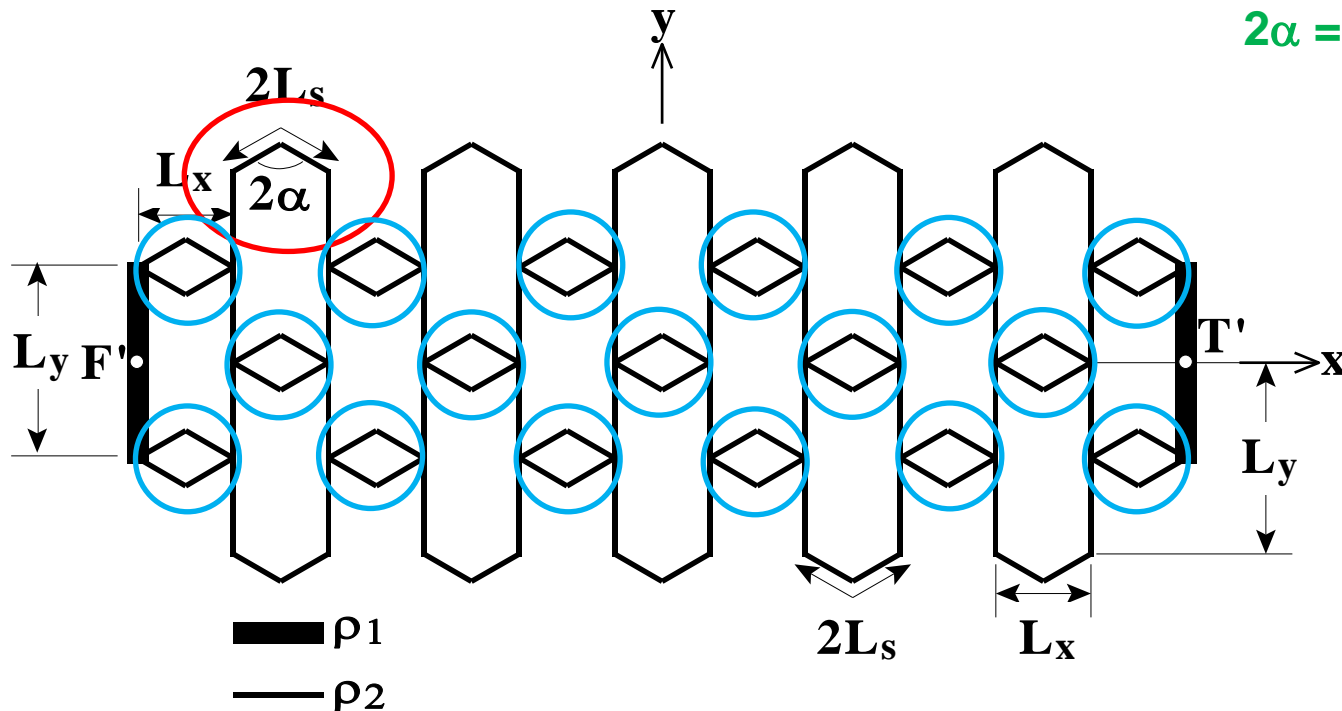
An extension of the conventional GAA.

Radiation Elements :: bent with bend angle 2α *

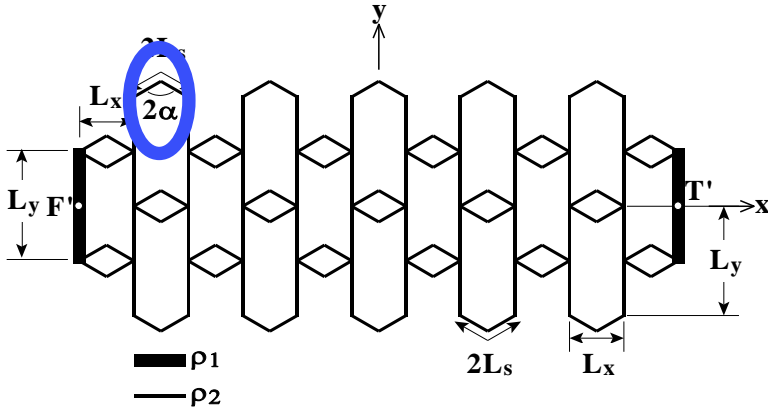
forming numerous rhombic cells.*

The conventional GAA : a special case , - - the bend angle : 180 degs.

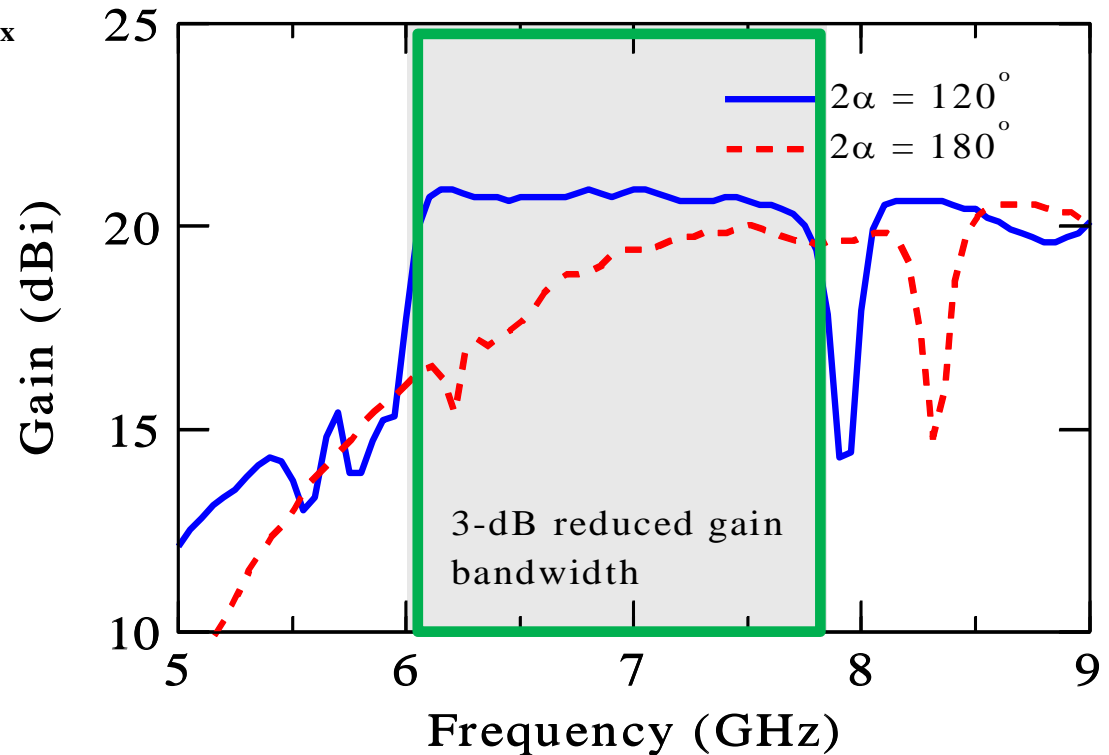
**Conventional
GAA
 $2\alpha = 180^\circ$**



*Gain for a **RGAA** -- bend angle of $2\alpha = 120^\circ$.*



Constant Gain
 across a wide frequency band

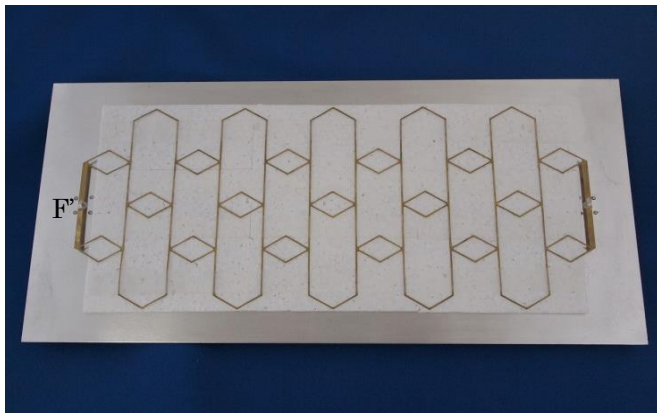


Note: -/ a constant gain across a wide frequency-band. *
 the gain for the conventional GAA using a red dotted line*
 : clear that the gain for beam scanning is improved.

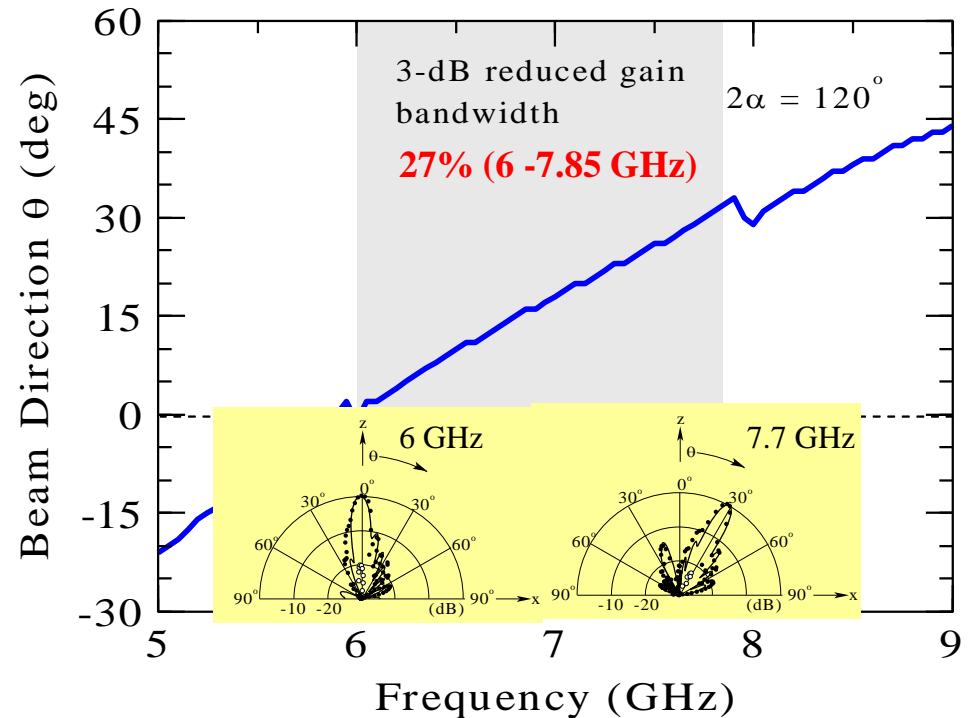
* Beam Direction for Bend Angle $2\alpha = 120^\circ$.

Note: the beam direction increases linearly with an increasing frequency.

.. Representative radiation patterns at 6 GHz* and 7.7 GHz *



GAA: $\sim 2.28\lambda_6 \times 5.2\lambda_6$
 GP: $150 \text{ mm} \times 325 \text{ mm}$
 $= 3\lambda_6 \times 6.5\lambda_6$



Details of this work

H. Nakano, Y.Iitsuka, J. Yamauchi, “Rhombic grid array antenna,”
 in IEEE Trans. AP, No.5, 2013 (in press)

Out line

Section I Introduction

Section II Natural TW antennas

II-A Low-profile, moderately wideband **helical antenna**

II-B Extremely wideband **fan-shaped antennas**
for a base-station and a portable handset

II-C Low-profile, extremely wideband ***BOR-SPR antenna**
for a base-station antenna

*Body of Revolution with a Shorted Parasitic Ring

II-D Low-profile, wideband **rhombic grid array antenna**
for frequency beam-scanning

Section III Metamaterial TW antennas

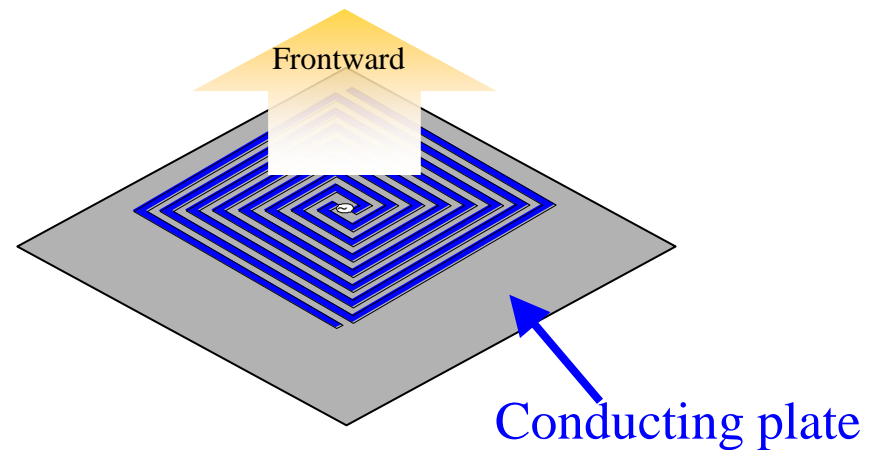
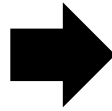
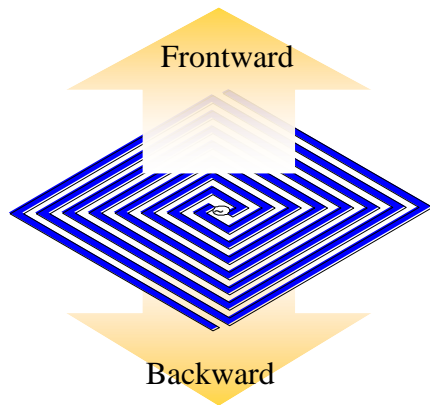
III-A History of the antenna height reduction of a spiral antenna

III-B Extremely low-profile, moderately wideband **spiral antenna**
for counter CP radiation

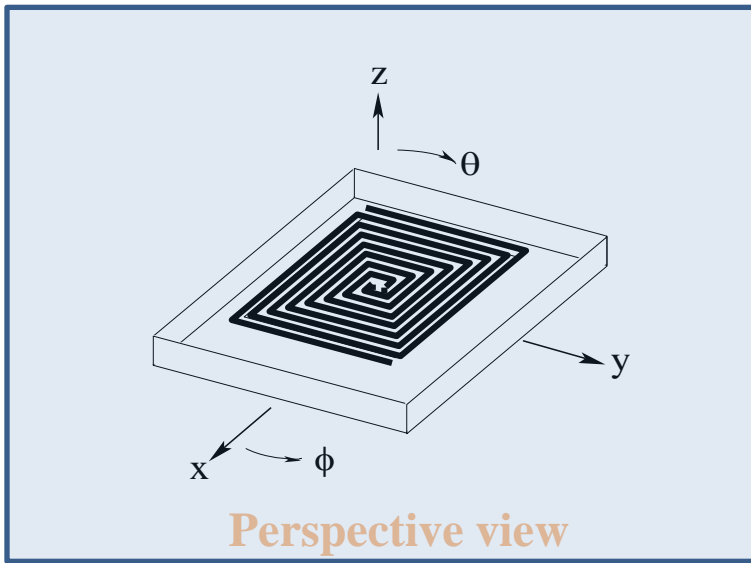
Section IV Remarks

Spiral Antenna

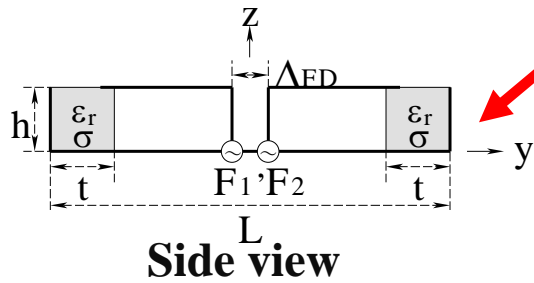
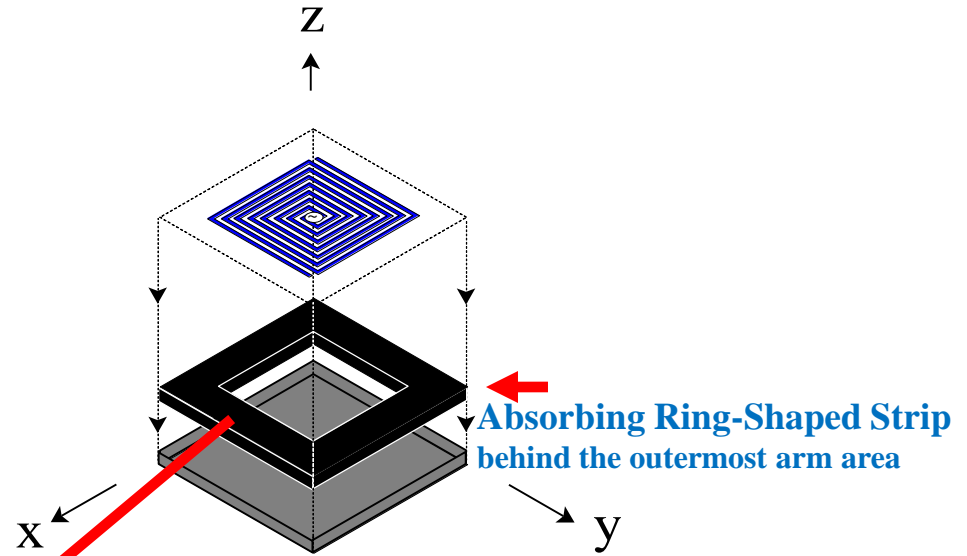
Bidirectional Circularly polarized (CP) wave



Unidirectional CP wave



First Technique

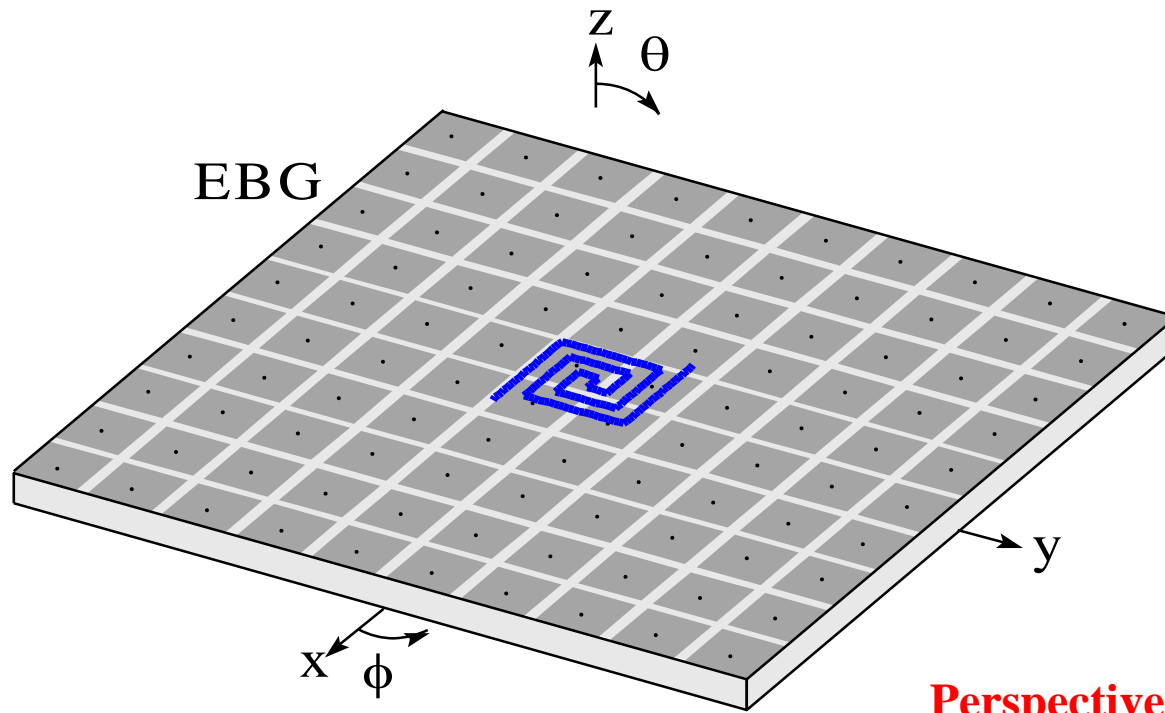


~:: Two Techniques to overcome::~~

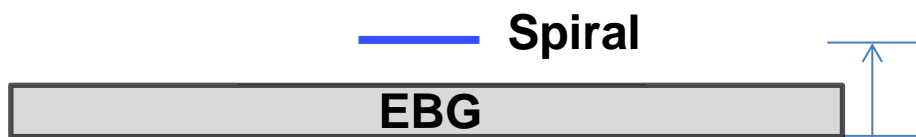
1st technique_ to place an absorbing ring-shaped strip*

Second Technique

: to replace the conducting plate by an EBG reflector *



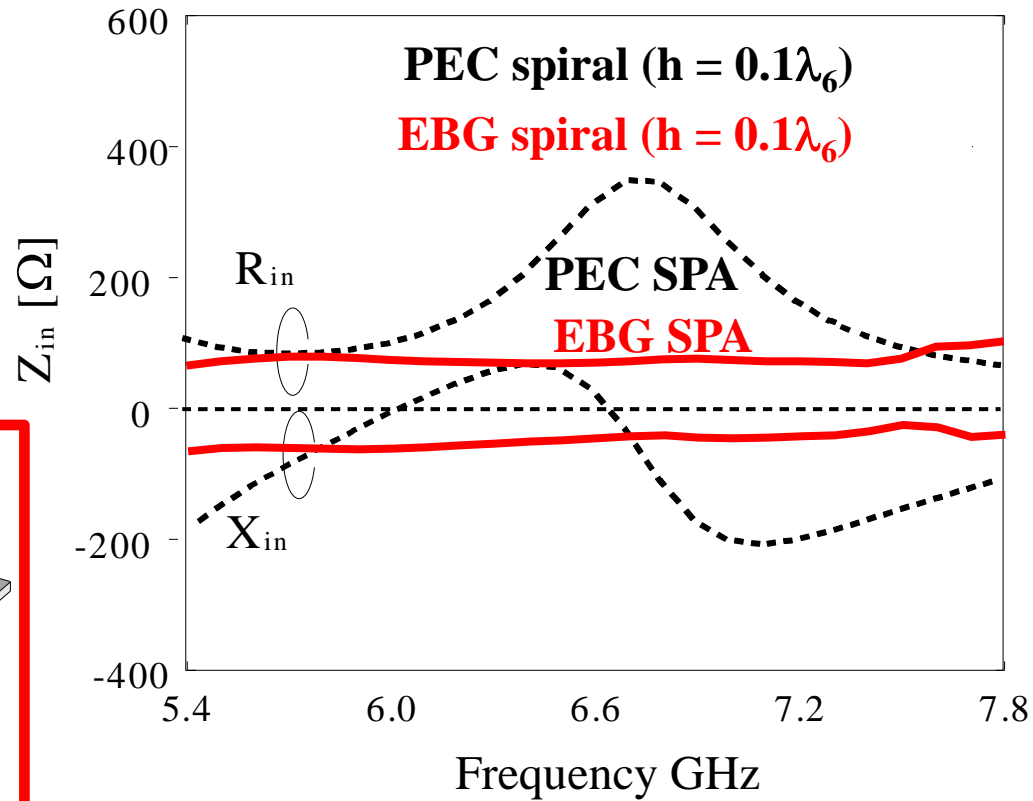
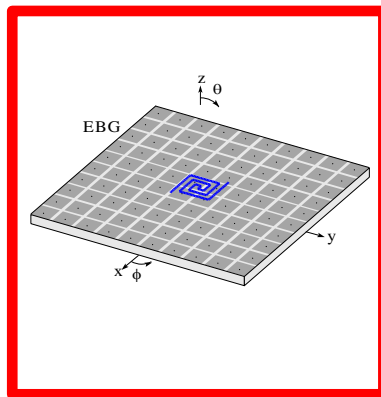
Perspective view



Side view

Antenna Height
 $\lambda/10$

.. / Effect of an EBG-Reflector on Z_{in}



Z_{in} becomes constant when the conducting plate is replaced by an EBG reflector.

Q

Antenna Height

Is it possible to
further reduce the height of
a spiral antenna from $\lambda/10$?

Out line

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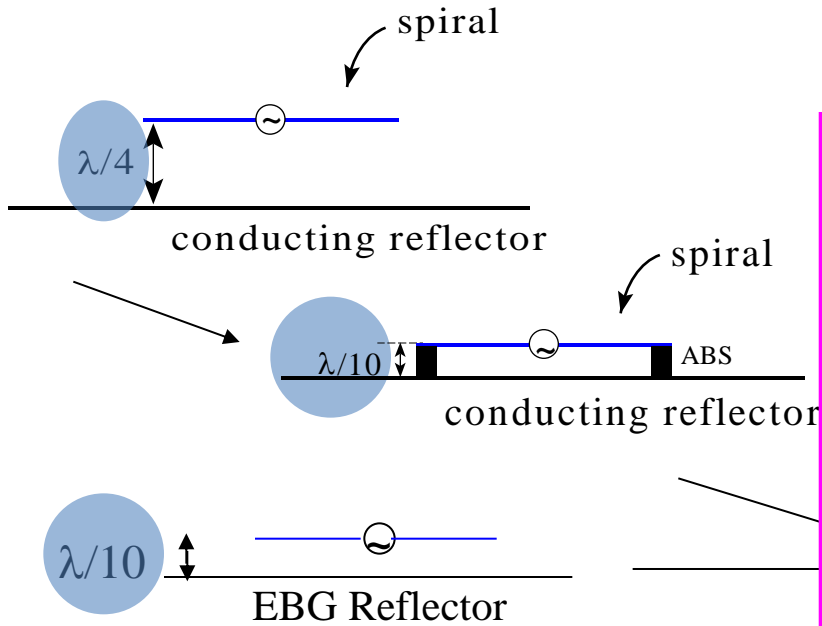
II-D Low-profile, wideband **rhombic grid array antenna**
for frequency beam-scanning

Section III Metamaterial TW antennas

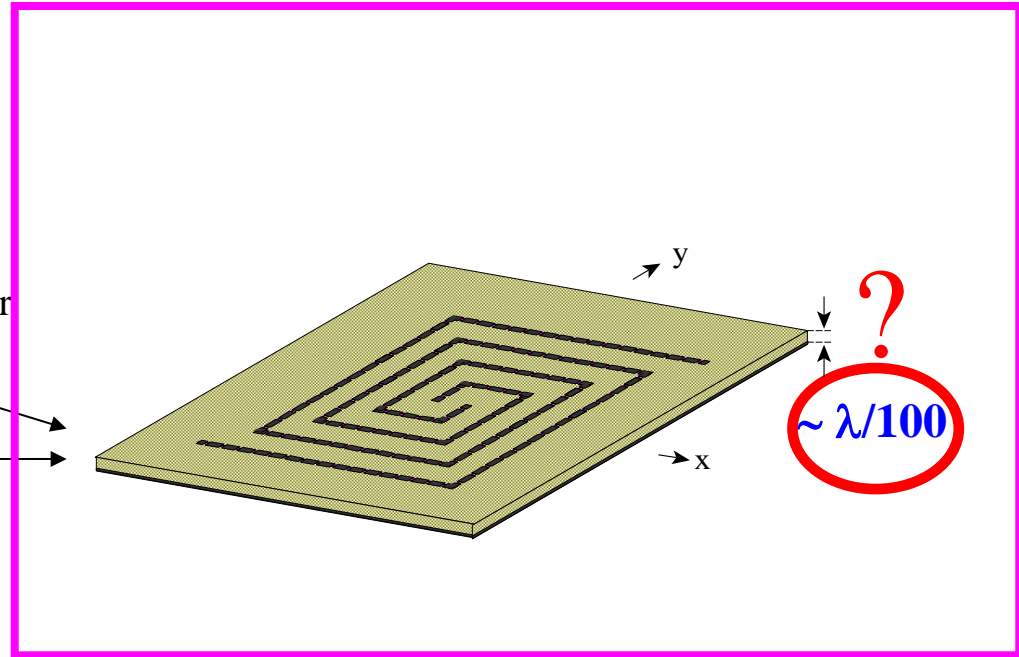
III-A History of the antenna height reduction of a spiral antenna

III-B Extremely low-profile, moderately wideband **spiral antenna**
for counter CP radiation

Section IV Remarks



.. CONSIDERATION
Further Antenna Height Reduction*

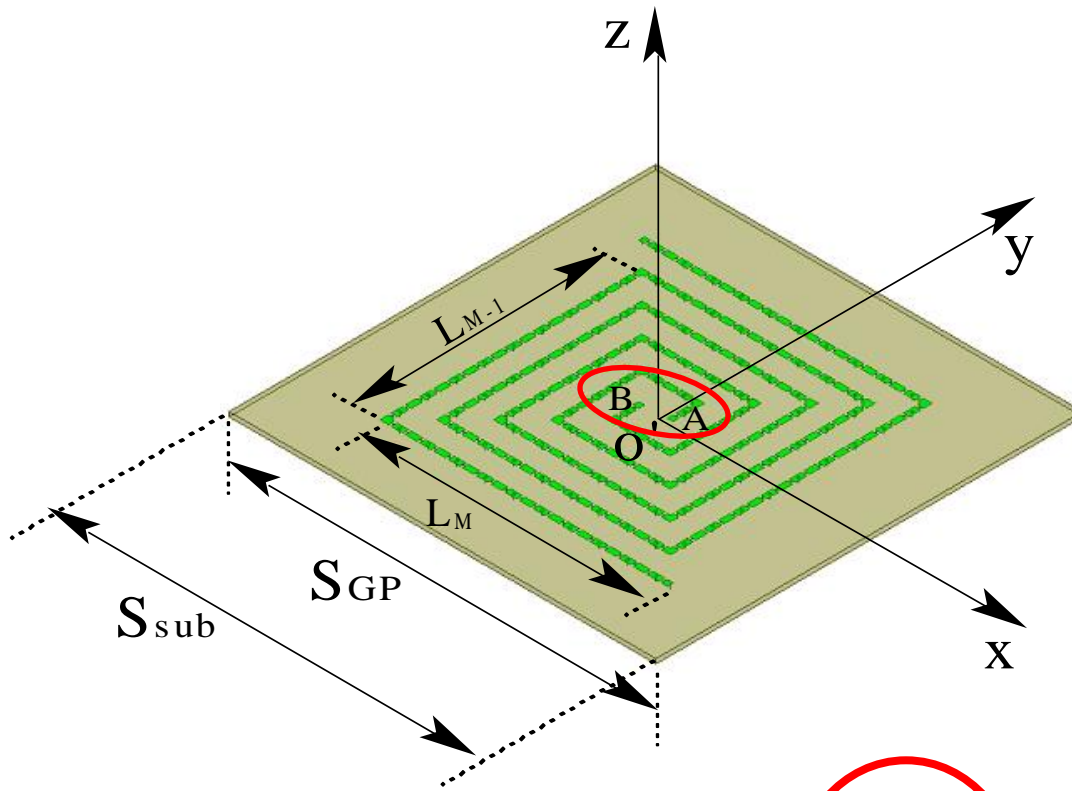


- - An antenna height of approximately $\lambda/100$

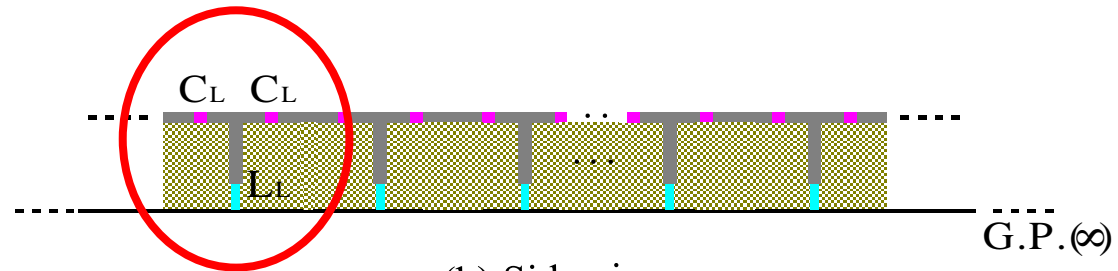
*Proposed Two-arm Spiral Antenna

– will be designed to meet two requirements.

1. Symmetrical Radiation Pattern
2. Extremely Low-profile Structure



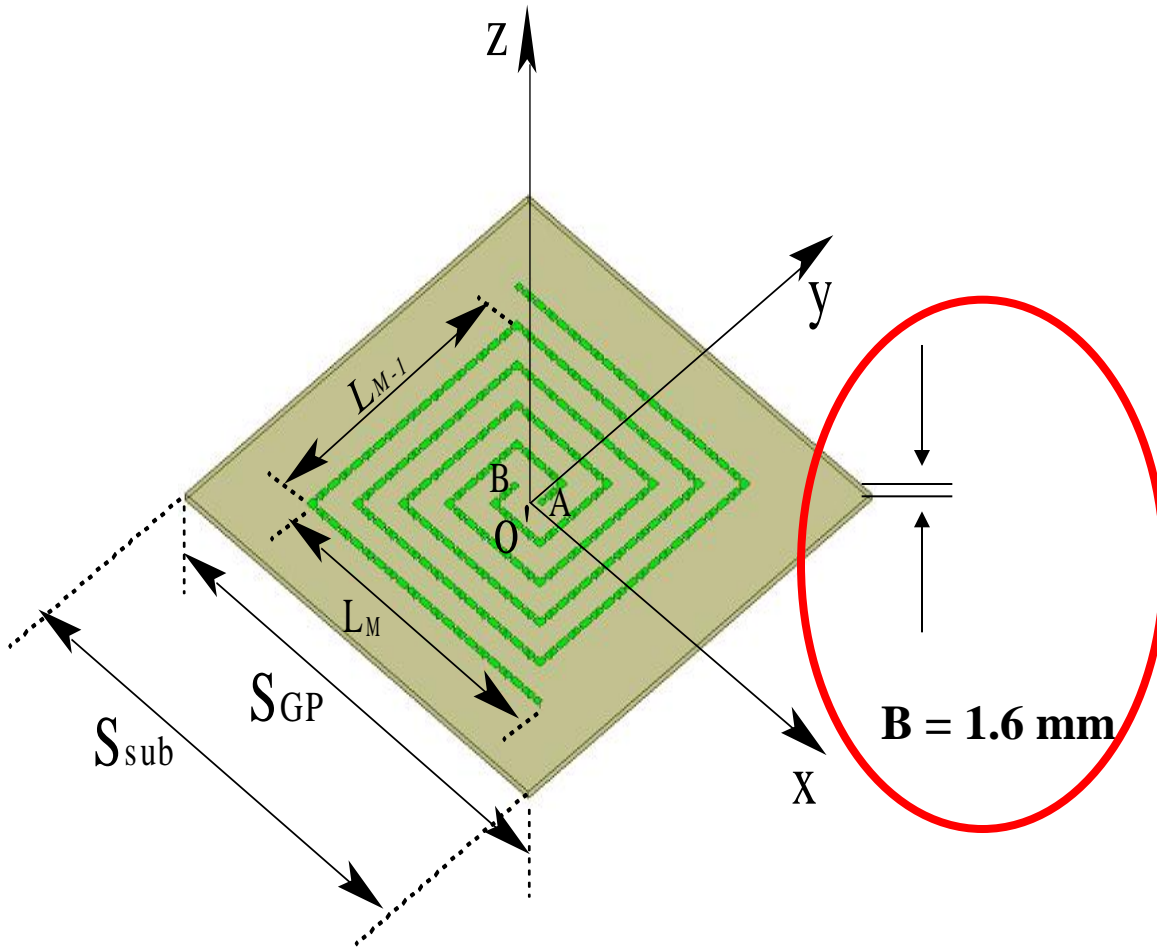
(a) Perspective view.



(b) Side view

- two feed points A and B *
- excited in balanced mode.
- **Antenna arms:** composed of numerous cells,
Cell * / two capacitors & one inductor.

Capacitors and inductor : : periodically added to the antenna arm.



1. Symmetrical Radiation Pattern

2. Extremely Low-profile Structure

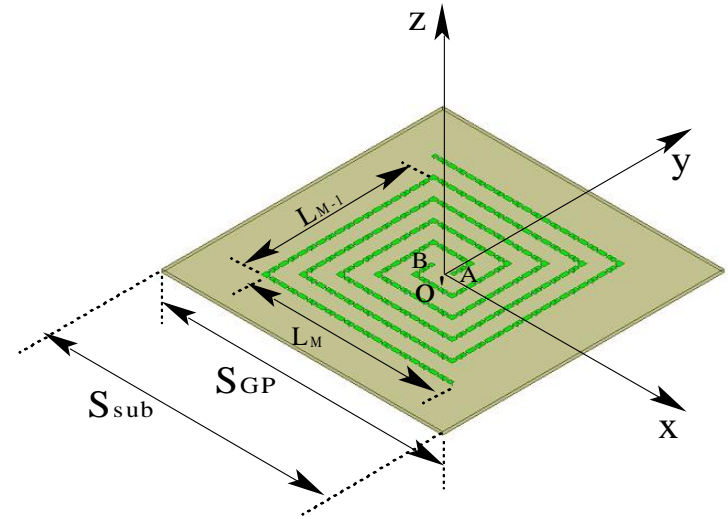
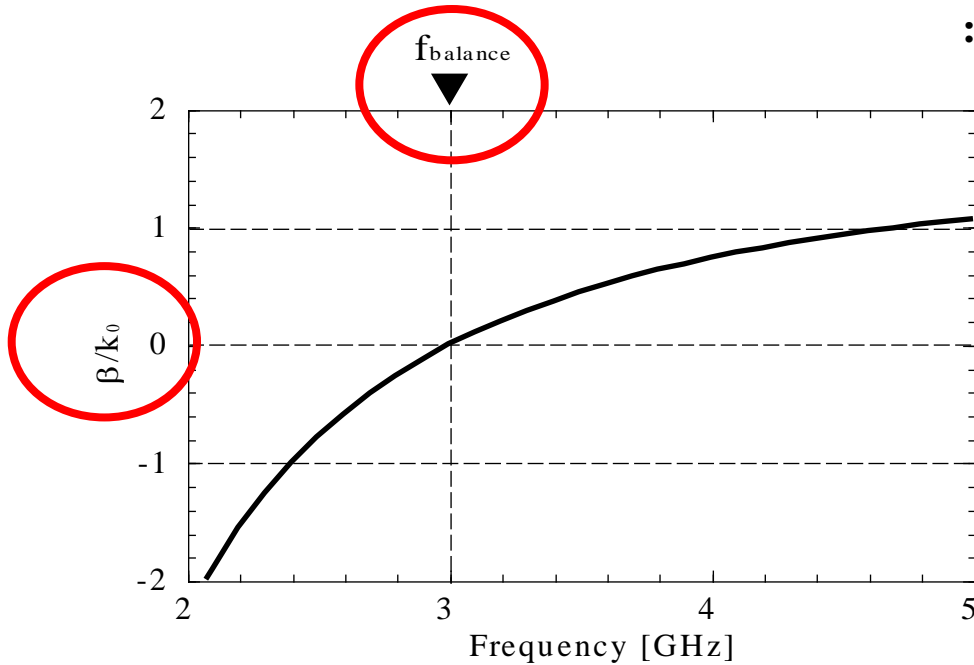
Perspective view.

.. An Antenna Height of 1.6 mm*

~ 0.013 wavelength at 2.5 GHz

*Dispersion Diagram from 2 GHz to 5 GHz

: Calculated Using Scattering Parameters [S]*



β : phase constant along the arms

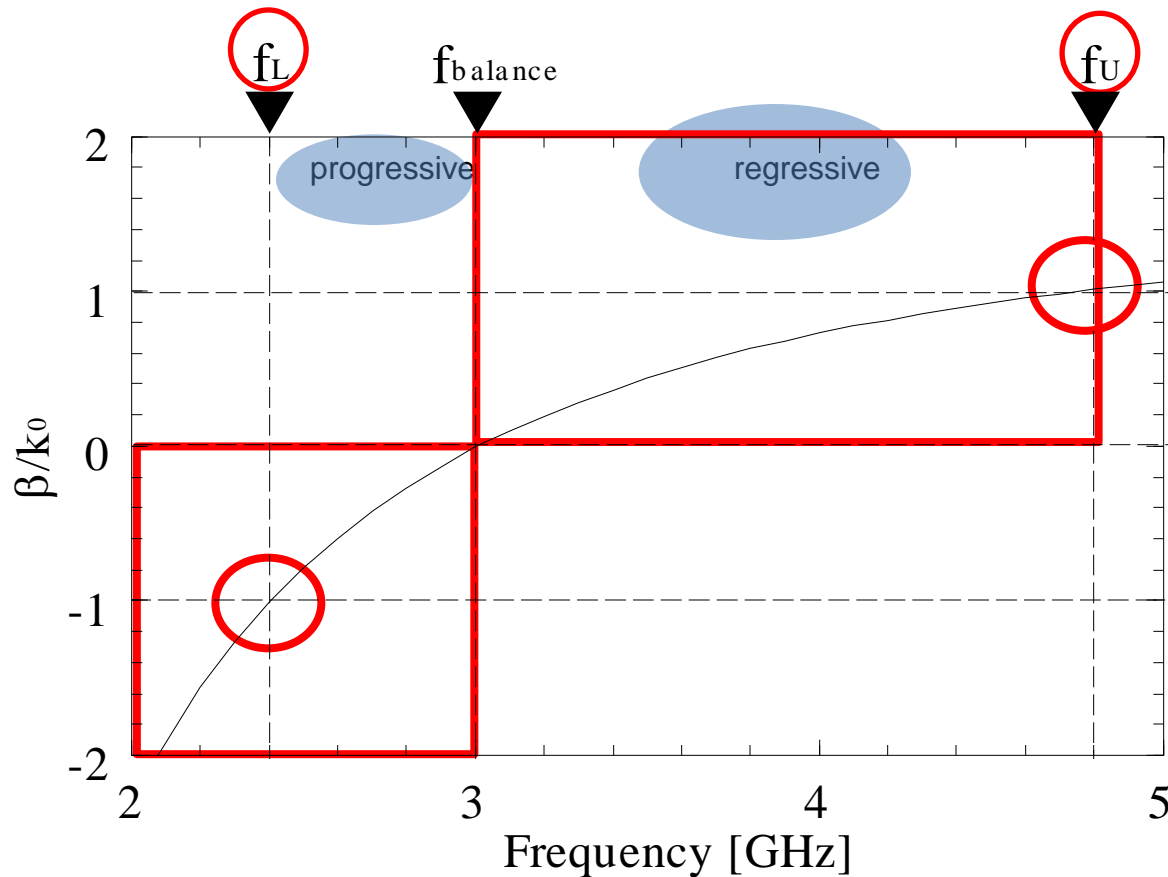
k_0 : phase constant in free space

f_{balance} : *balanced frequency : chosen to be 3 GHz

Dispersion Diagram

f_L : lower bound for a fast wave*

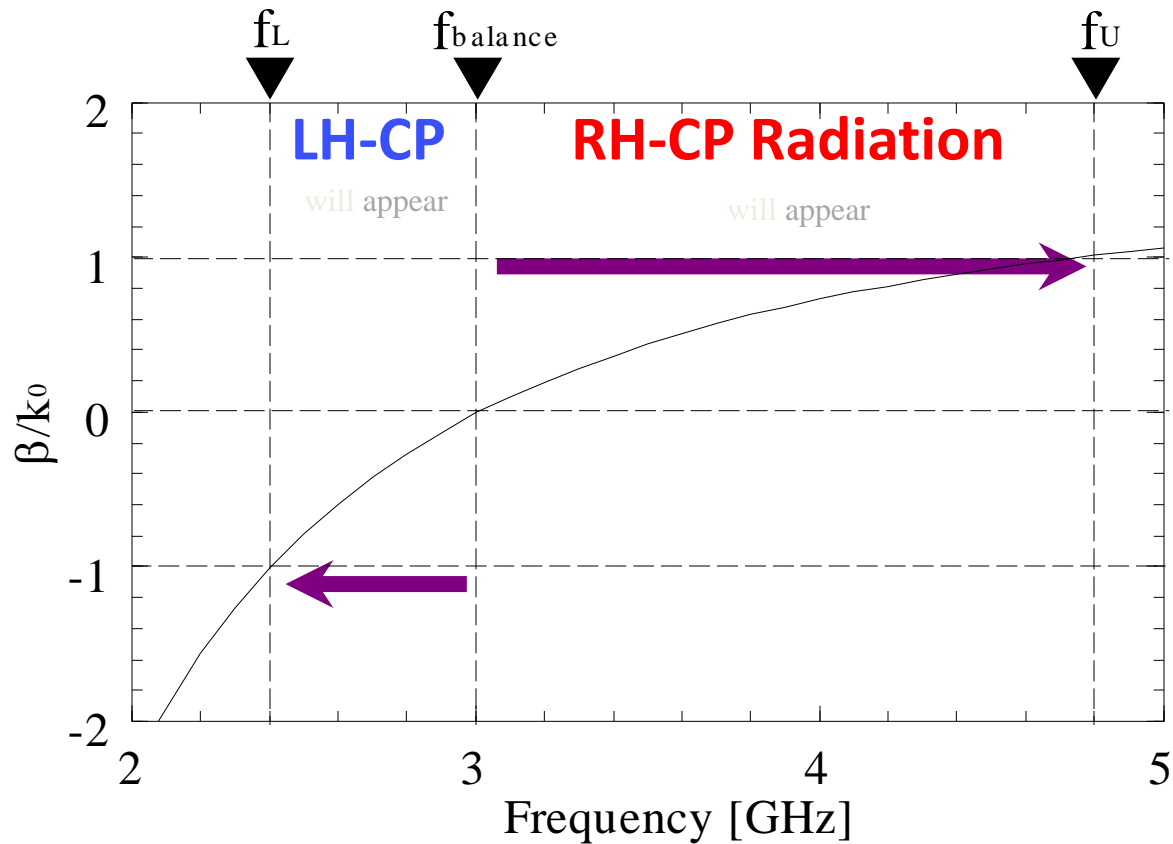
f_U : upper bound for a fast wave*



@ f_L^* , $\beta/k_0 = -1$

@ f_U^* , $\beta/k_0 = +1$

// Dual-band Counter-CP Radiation//
If the antenna size is appropriately chosen

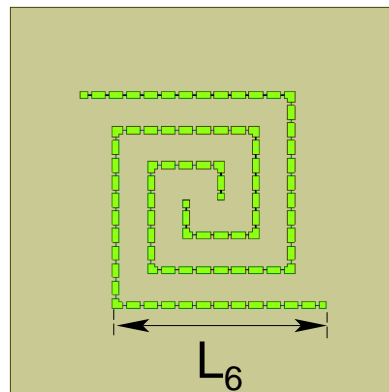


Design

.. An MTM Spiral having 6 Filaments.

~ The MTM spiral operates in the first mode.

Moderately wide-band characteristics:: Expected



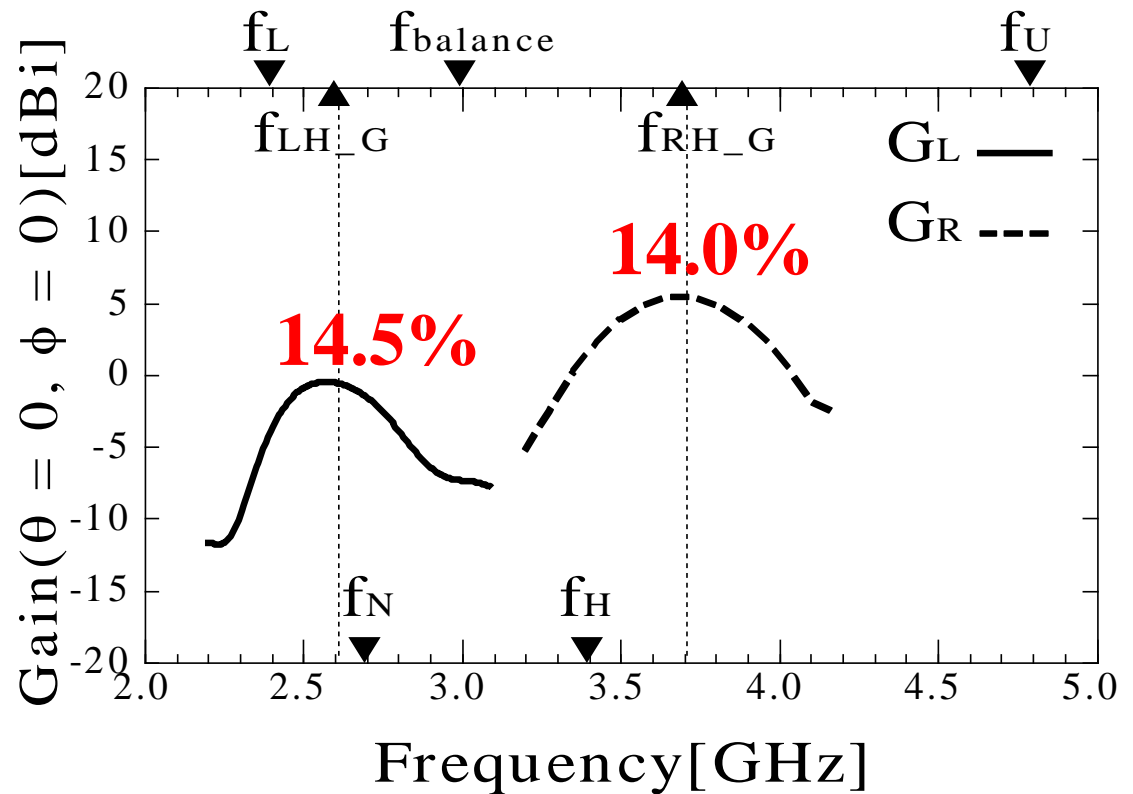
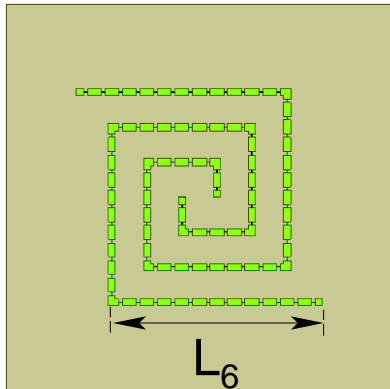
$$L_6 = 6 \text{ cm} = 0.5\lambda_{2.5}$$

* Frequency response of the gain

The maximum **LH CP gain** appears near the N-frequency.

The maximum **RH CP gain** appears near the H-frequency.

$M = 6$

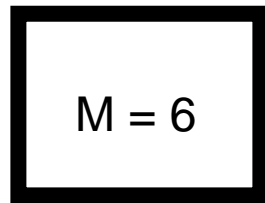
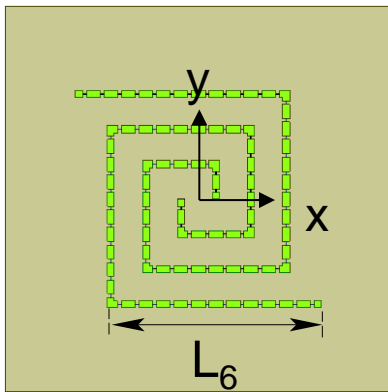
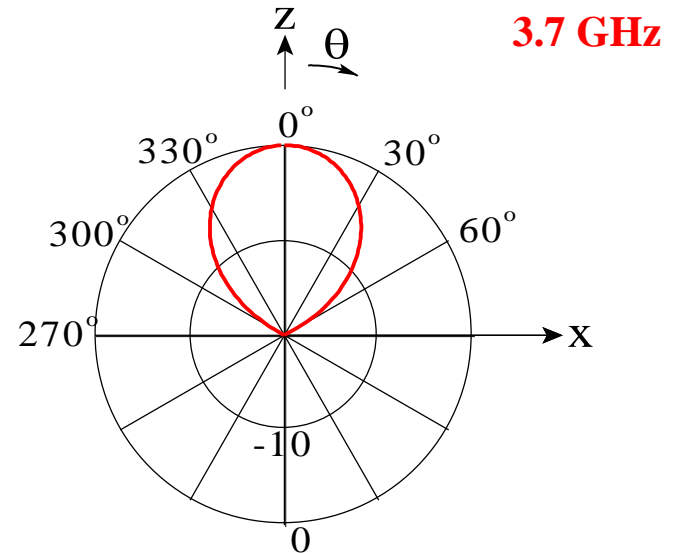
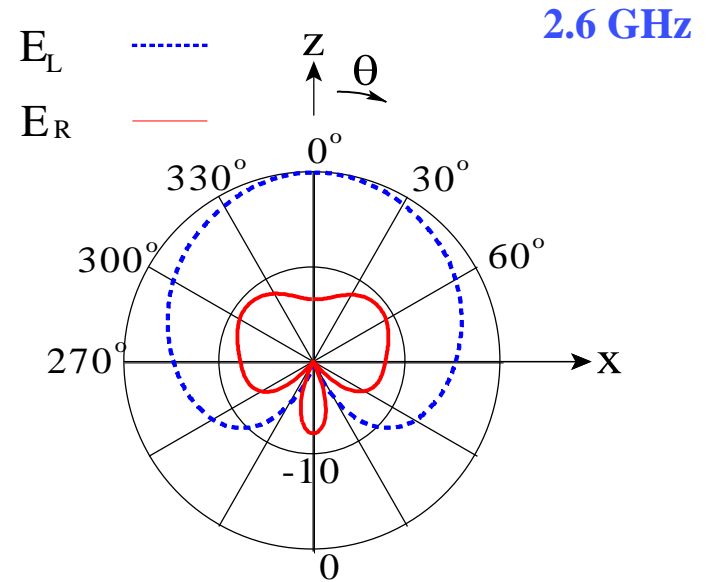
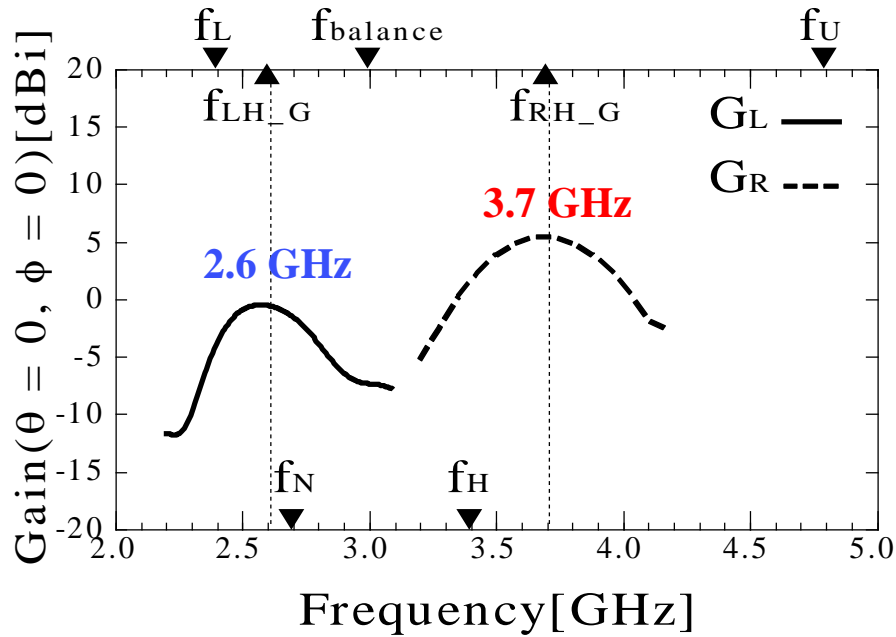


The gain has a moderately wideband characteristic
~ meets one of the requirement 2.

Purposes

1. Symmetrical Radiation Pattern
2. Moderately Wideband Characteristics

Radiation Pattern

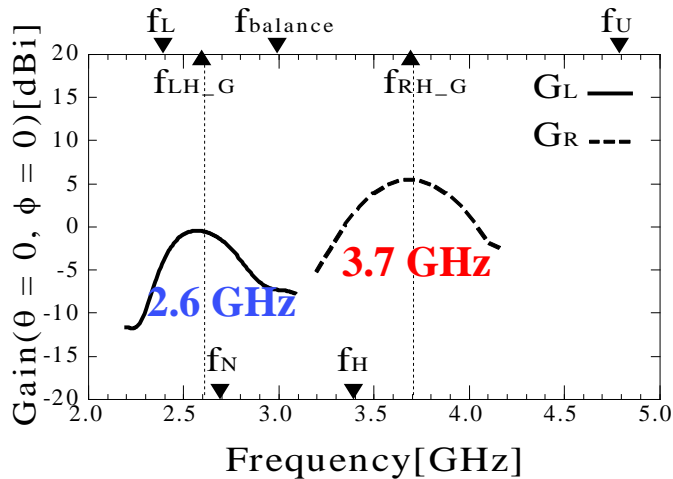
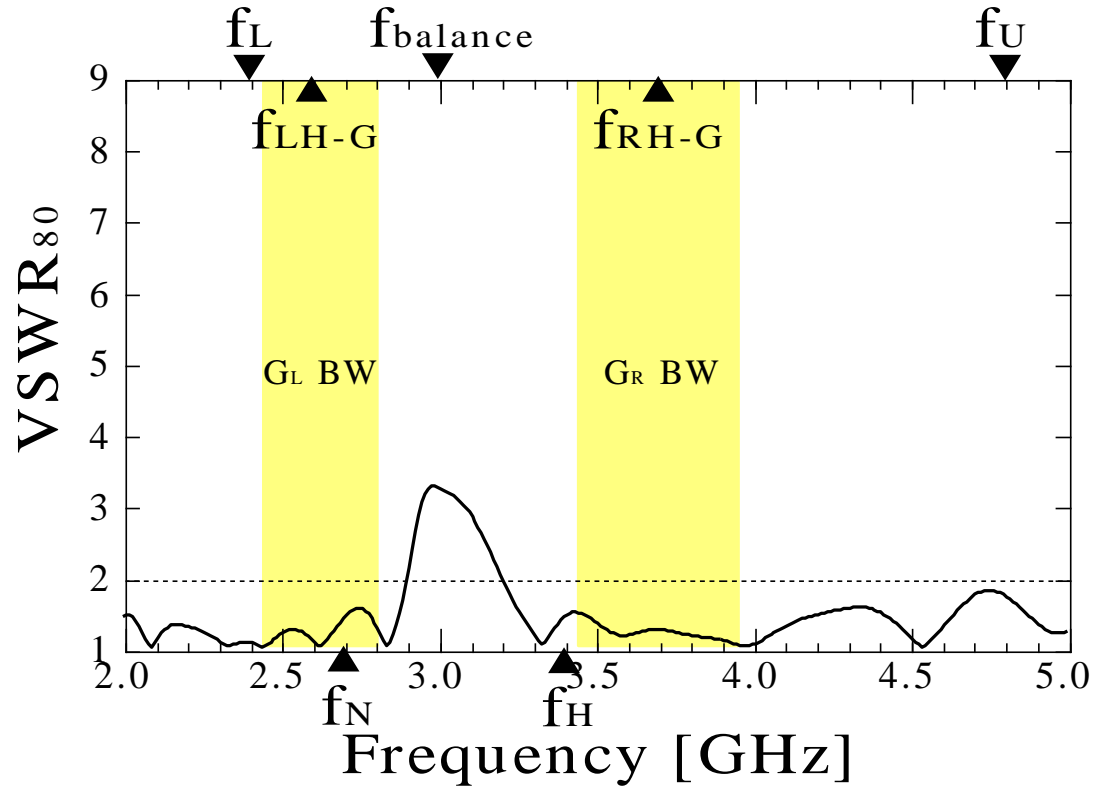
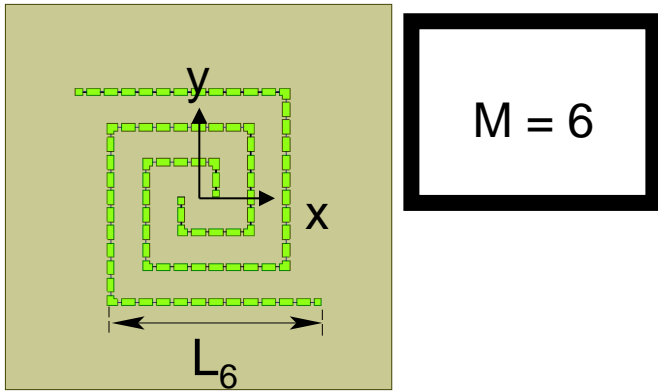



Purposes

1. Symmetrical Radiation Pattern
2. Moderately Wideband Characteristics

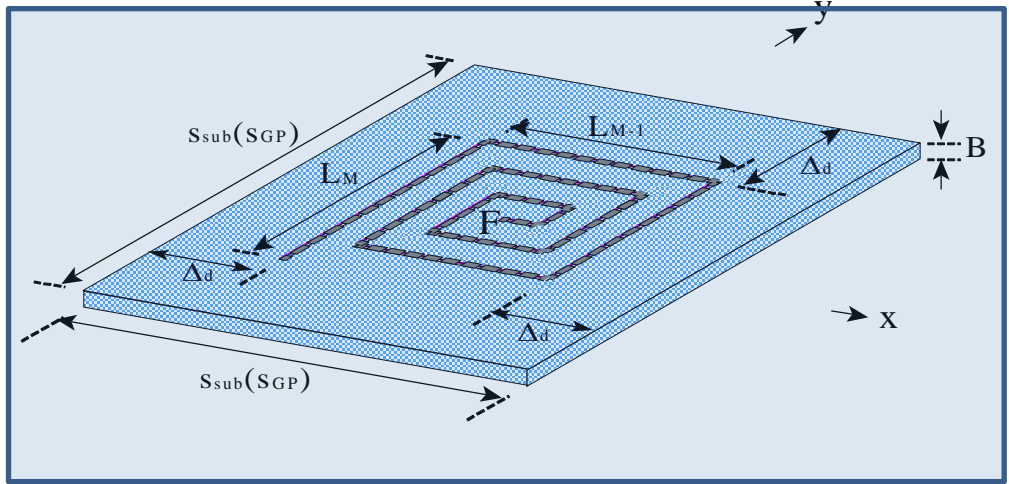
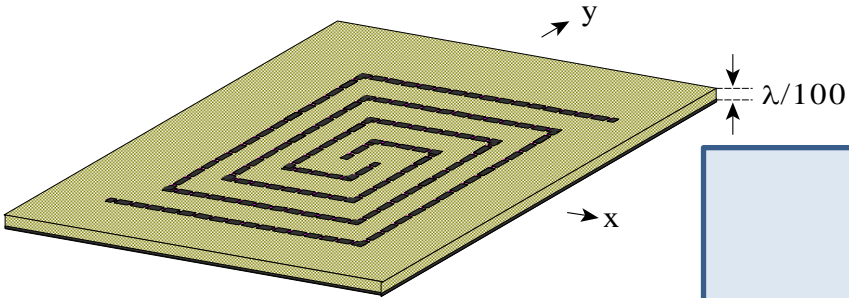
- : symmetrical with respect to the z-axis

Frequency response of the VSWR for $M = 6$ *



 3 dB-reduction Gain Band Width

The VSWR : less than 2 within the gain bandwidth



Two-Arm MTM Spiral*

Current Work

A Monofilar MTM Spiral

- does not require a balun circuit
- -
- Effects of the pitch and ground plane on the antenna characteristics :: *

Details of this work

Dual-band Counter Circularly Polarized Radiation from a Single-arm Metamaterial-based Spiral Antenna

in IEEE Trans AP, June, 2013 (accepted for publication)

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REMARKS

Antenna Height from $\lambda/4$ to $\lambda/100$

**An incoming current should be reduced
to realize a wideband antenna.**

**Some natural antennas, specified by a positive- β current,
realize wideband characteristics,
having a low profile structure.**

**The antenna height can be reduced
using a metamaterial property,
which is featured by a negative- β current.**